

Criteria to Protect Telecommunication Cabling During a Power Cross Event



Presented by:

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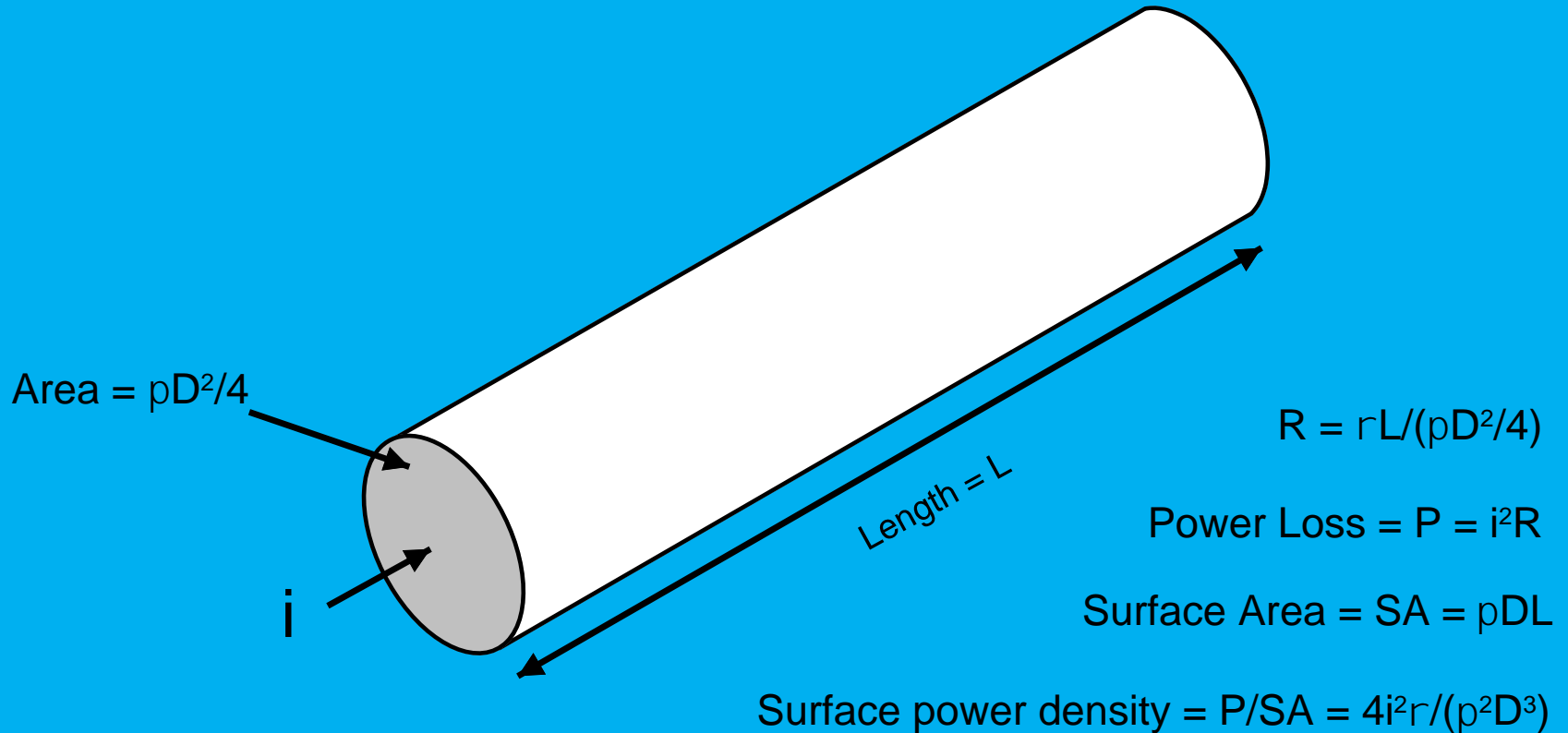
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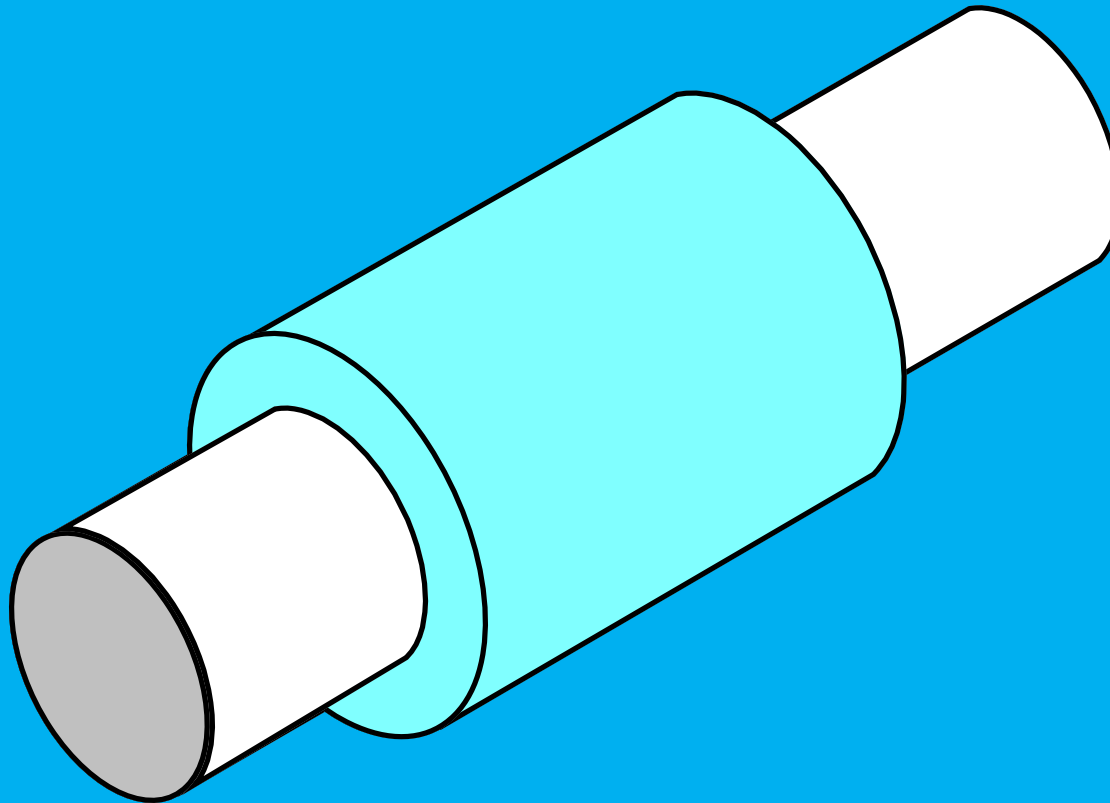
Rational for this work

- North American standards, UL 60950-1 and GR-1089-CORE, test for power fault wiring damage.
- International standards, IEC and ITU-T, don't test for power fault wiring damage.
- This work created ITU-T Supplement 3 (2015): *ITU-T K.20, K.21, K.45 and K.82 – Additional criteria to protect telecommunication cabling during a power cross event*

Just a piece of wire



Insulation damage sets temperature limit



DC fusing current of wires in free air (Preece)

$$I = A * d^{1.5}$$

Where I is the wire fusing current, d is the wire diameter and A is a constant, dependent of units system and the wire material. For a copper wire of diameter of d mm, the equation becomes:

$$I = 80 * d^{1.5}$$

For example, 32 AWG has a diameter of 0.2019 mm, making $I = 80 * 0.2019^{1.5} = 7.3$ A.

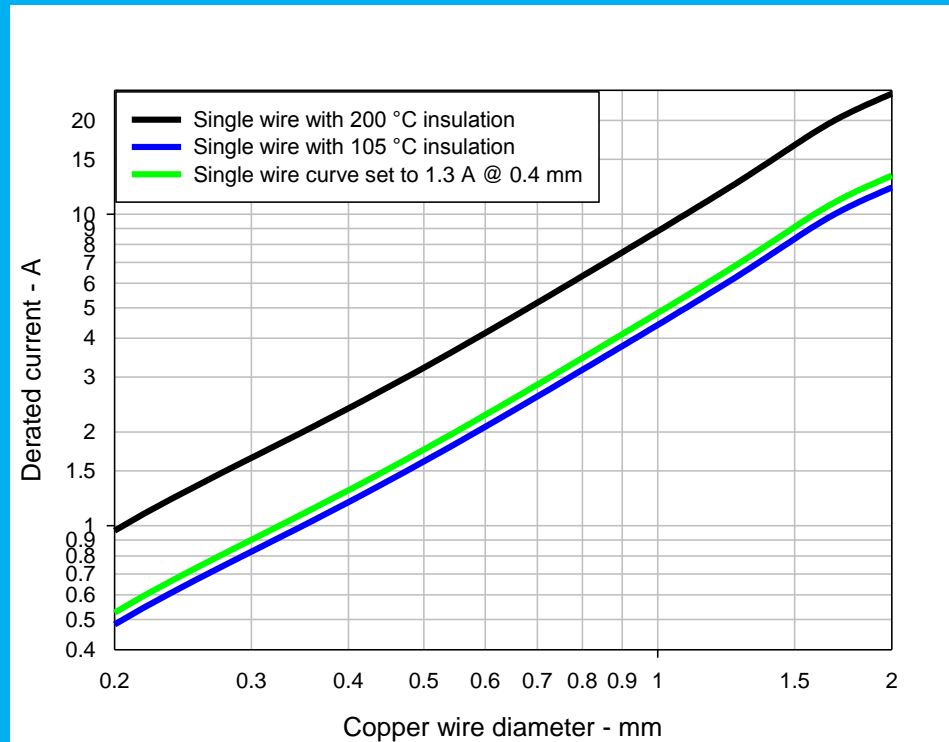
Preece W. H., *On the Heating Effects of Electric Currents*, Proc. Royal Society 36, 464 - 471 (1883). No. II, 43, 280 - 295 (1887). No. III, 44, 109 - 111 (1888).
(Retrieved 2015-09 from www.ultracad.com/articles/reprints/preece.zip)

DC Insulation damage current

- MIL-STD-975 section 3.16 Wire and Cable Derating Criteria gives maximum currents for an ambient of 70 °C and various insulator maximum temperatures (Teflon at 200 °C down to types of PVC at 105 °C).
- For cable bunches, a derating factor of $(28-N)/27$ should be applied, where N is the number of conductors. The derating factor is taken as a constant value once the bundle exceeds fifteen conductors.

MIL-STD-975M NASA, Standard Electrical, Electronic and Electromechanical (EEE) Parts List, 5 August 1994

DC levels to avoid insulation damage



MIL-STD-975 derated current versus wire diameter

Adiabatic (thermal capacity) conditions Onderdonk equation

$$I^2t = 7.28 * 10^4 * d^4 * LOG\left(\frac{\Delta T}{274} + 1\right)$$

Where

I (A) is the wire current,

d (mm) is the wire diameter,

t (s) is the current flow time, and

ΔT is the temperature difference (°C) between the wire and ambient.

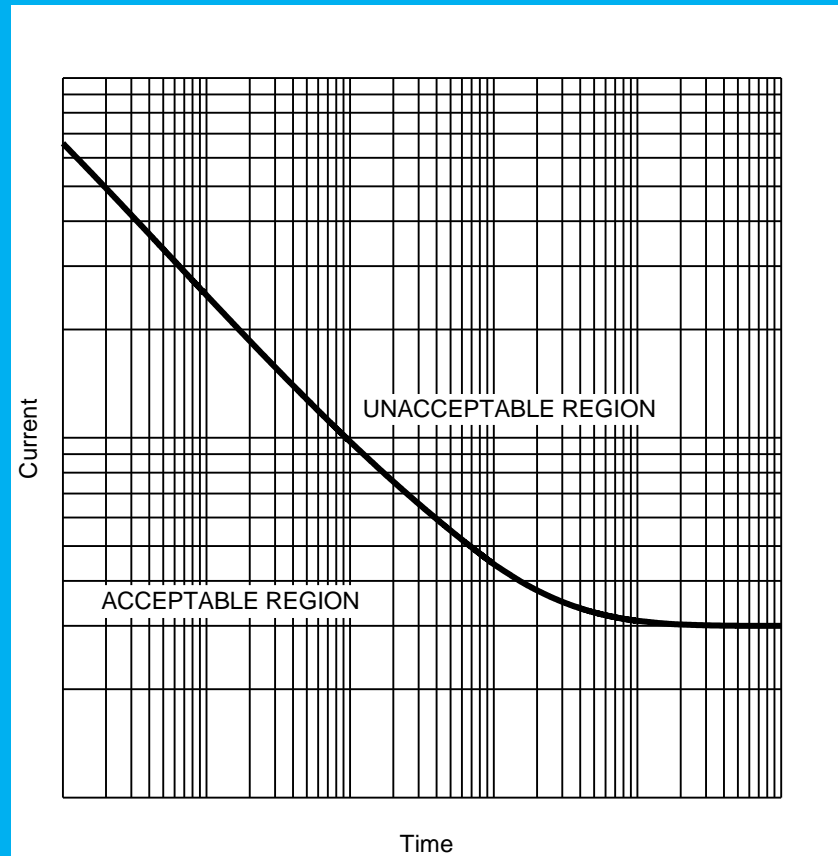
For an ambient of 30 °C and the copper melting temperature of 1083 °C, the equation becomes:

$$I^2t = 5 * 10^4 * d^4$$

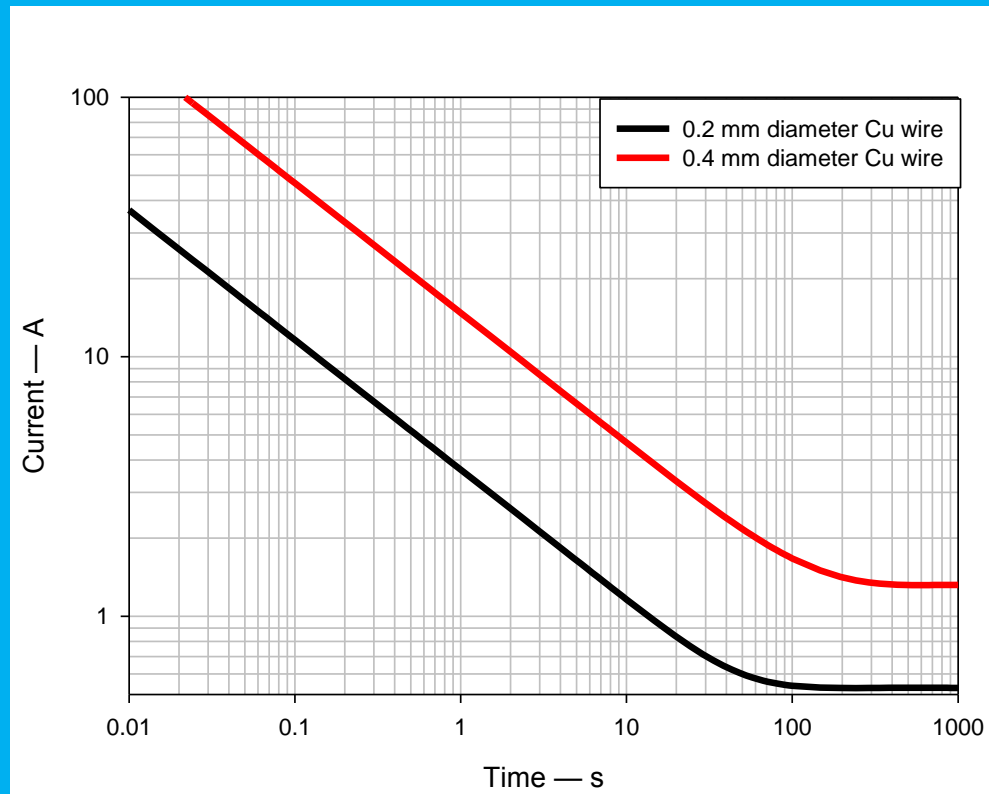
Adam J. & Brooks D., In Search for Preece and Onderdonk, 2015 (retrieved 2015-09
<http://www.ultracad.com/articles/preece.pdf>)

ANSI/ICEA PUBLICATION P-32-382-2007, Short circuit characteristics of insulated cables

Typical wire current-time curve



Insulation damage limit current-time curve for 0.2 mm and 0.4 mm copper wire



Based on the P-32-382 i^2t values and the IEC 60950 equivalent DC values from Table I1 in Appendix I.

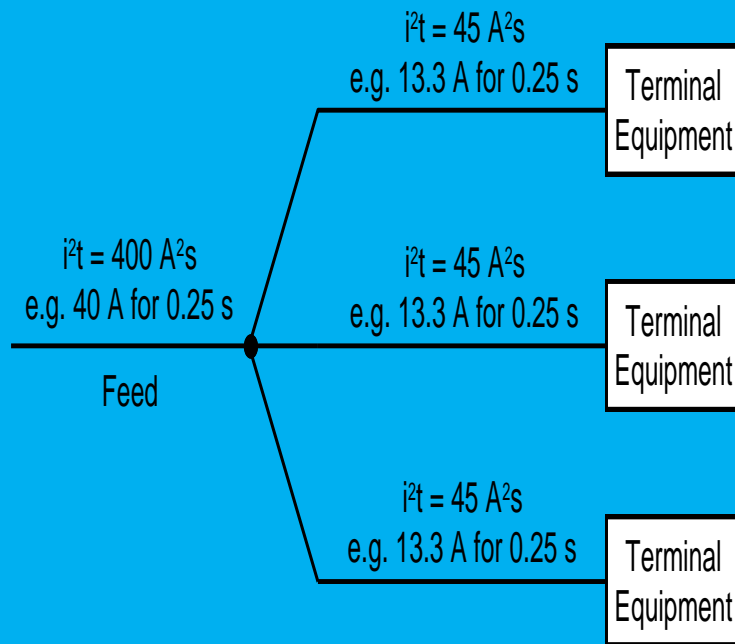
Parameters for 18 to 32 AWG

| Wire AWG | Dia (mm) | Preece DC Fusing (A) | Onderdonk transient melting i^2t (A ² s) | ICEA standard P-32-382 i^2t (A ² s) | IEC 60950-1 DC Figure I.1 (A) |
|-------------|-----------------|-------------------------------|--|---|--|
| 18 | 1.0237 | 82.7 | 64787 | 8881 | 4.99 |
| 19 | 0.9116 | 69.5 | 40745 | 5588 | 4.19 |
| 20 | 0.8118 | 58.4 | 25625 | 3516 | 3.53 |
| 21 | 0.7229 | 49.1 | 16116 | 2212 | 2.98 |
| 22 | 0.6438 | 41.2 | 10135 | 1392 | 2.51 |
| 23 | 0.5733 | 34.7 | 6374 | 876 | 2.13 |
| 24 | 0.5106 | 29.1 | 4009 | 551 | 1.81 |
| 25 | 0.4547 | 24.5 | 2521 | 347 | 1.54 |
| 26 | 0.4049 | 20.6 | 1586 | 218 | 1.32 |
| 27 | 0.3606 | 17.3 | 997 | 137 | 1.14 |
| 28 | 0.3211 | 14.5 | 627 | 86.3 | 0.98 |
| 29 | 0.2859 | 12.2 | 394 | 54.3 | 0.85 |
| 30 | 0.2546 | 10.3 | 248 | 34.2 | 0.73 |
| 31 | 0.2268 | 8.61 | 156 | 21.5 | 0.63 |
| 32 | 0.2019 | 7.24 | 98 | 13.5 | 0.53 |

Evolution of North American wiring simulators

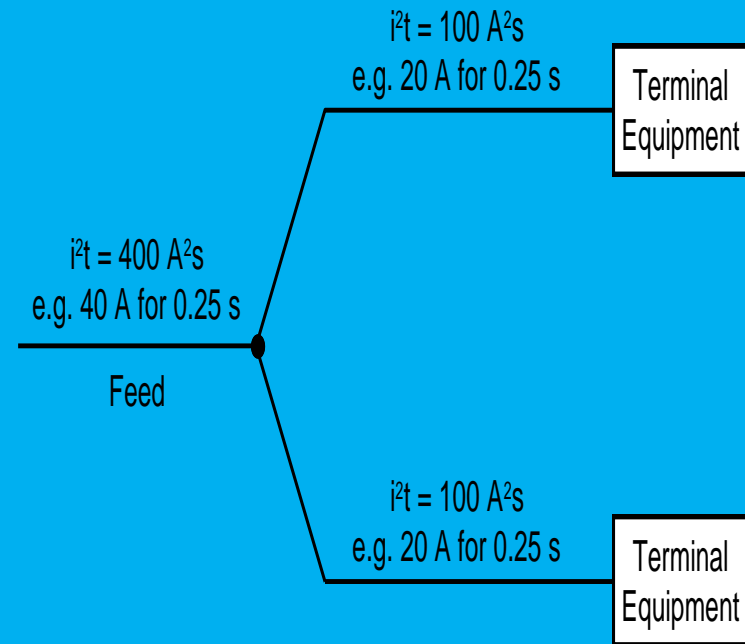
- ANSI/TIA/EIA-571 and ANSI/TIA/EIA-571A
- UL 1459-1998
- UL 60950-1
- GR-1089-CORE, Issue 6
- Stub links and block cable

EIA-571(A), 1992 (1999), Telecommunications User Premises Equipment Environmental Considerations – current division



571 Branches

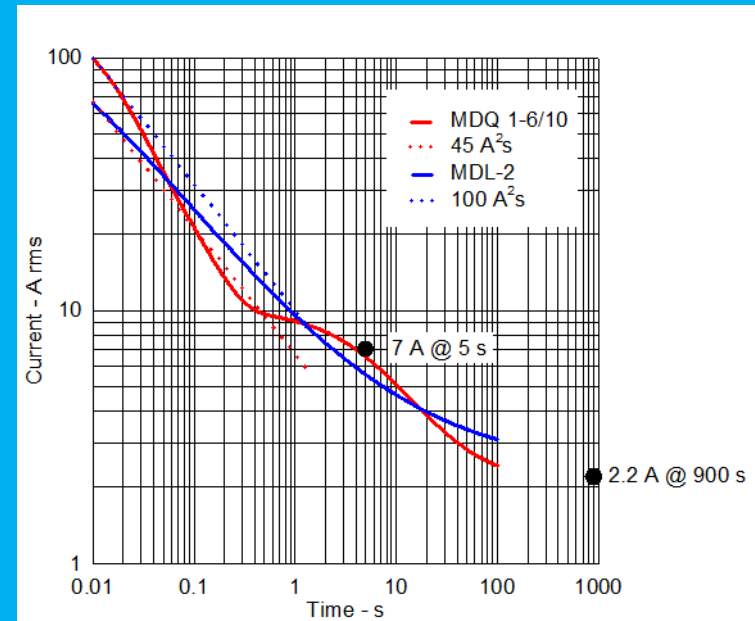
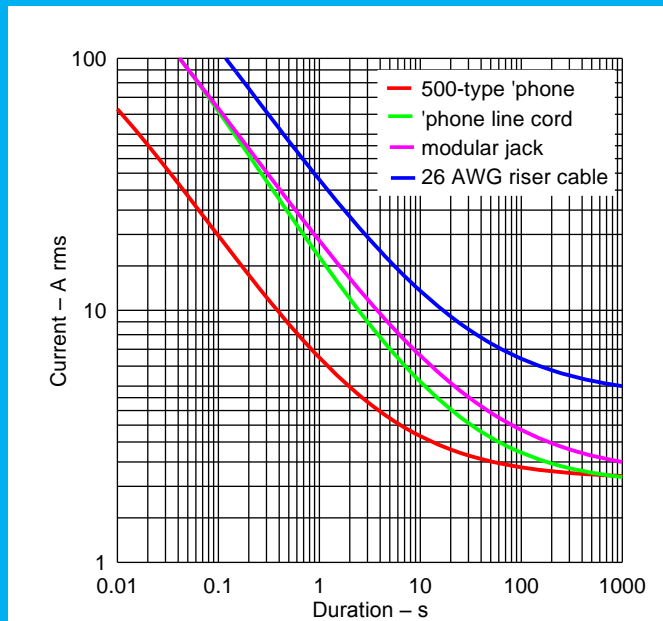
(a)



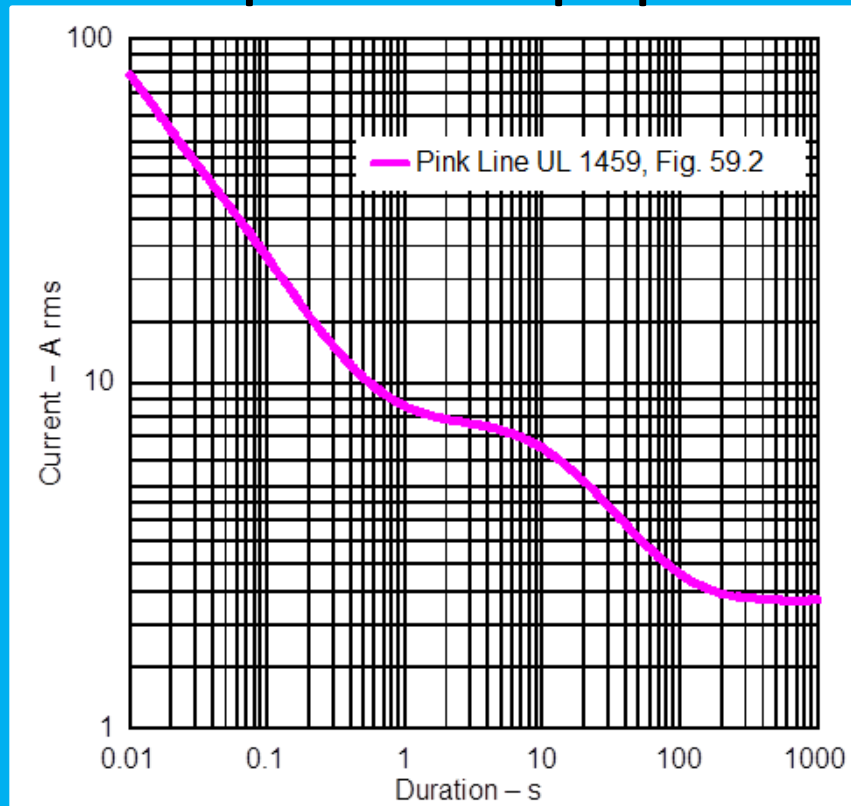
571-A Branches

(b)

EIA-571(A), 1992 (1999), Telecommunications User Premises Equipment Environmental Considerations – I-t curves

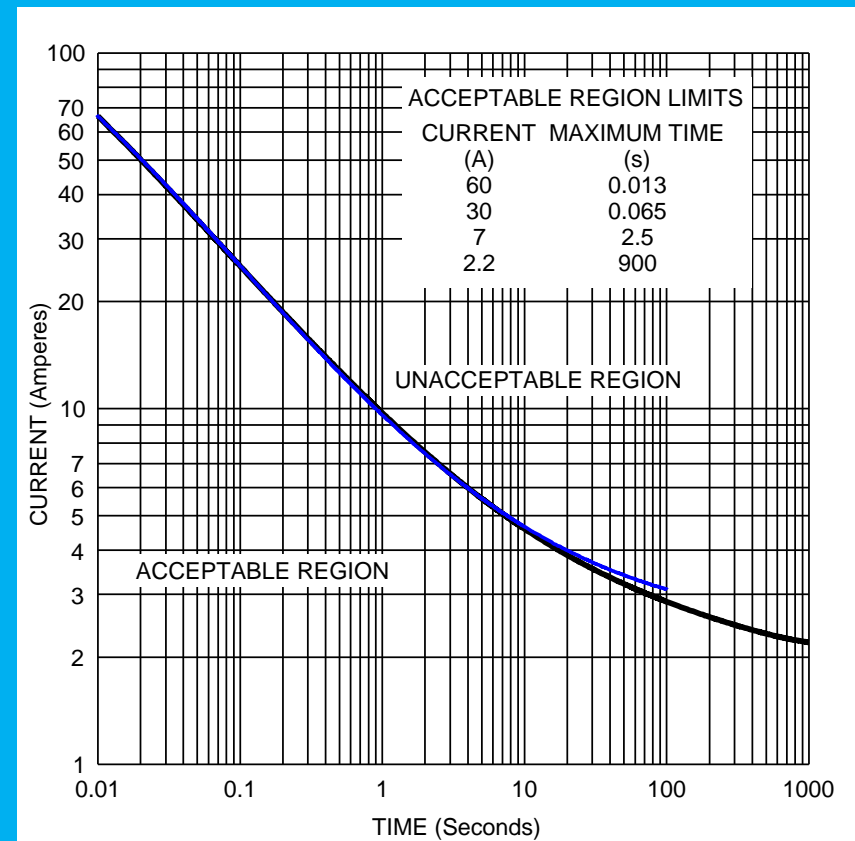
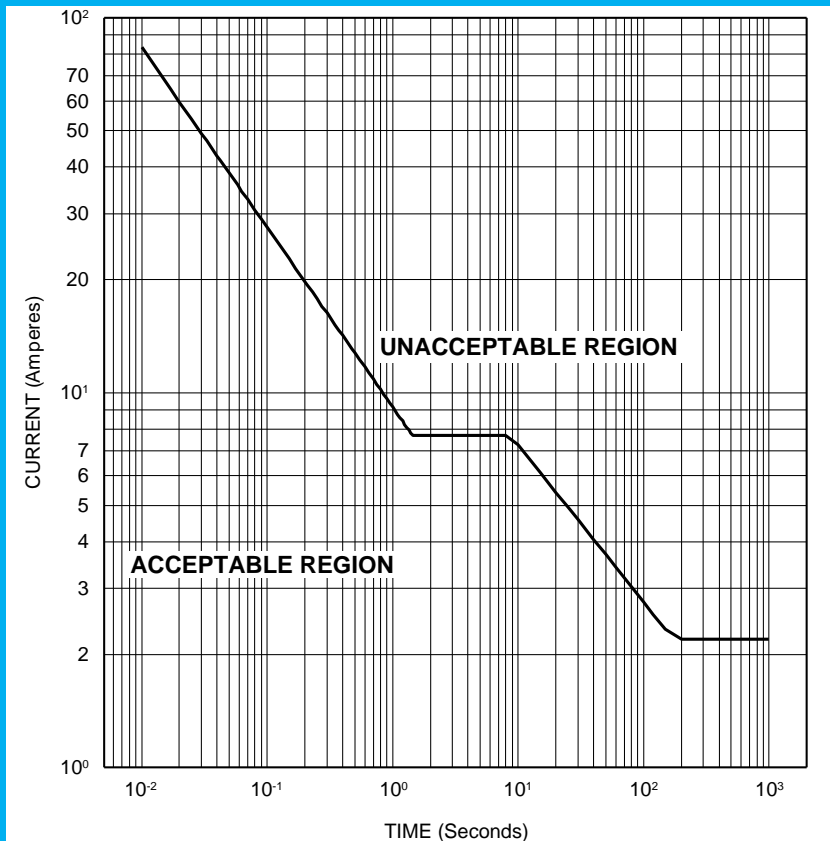


UL 1459 (1995): UL standard for safety - telephone equipment



UL 60950-1: Information Technology Equipment - Safety - Part 1: General Requirements used an MDL-2 fuse

GR-1089-CORE, Issue 6, 2011, Electromagnetic Compatibility and Electrical Safety - Generic Criteria for Network Telecommunications Equipment



Stub links and block cable

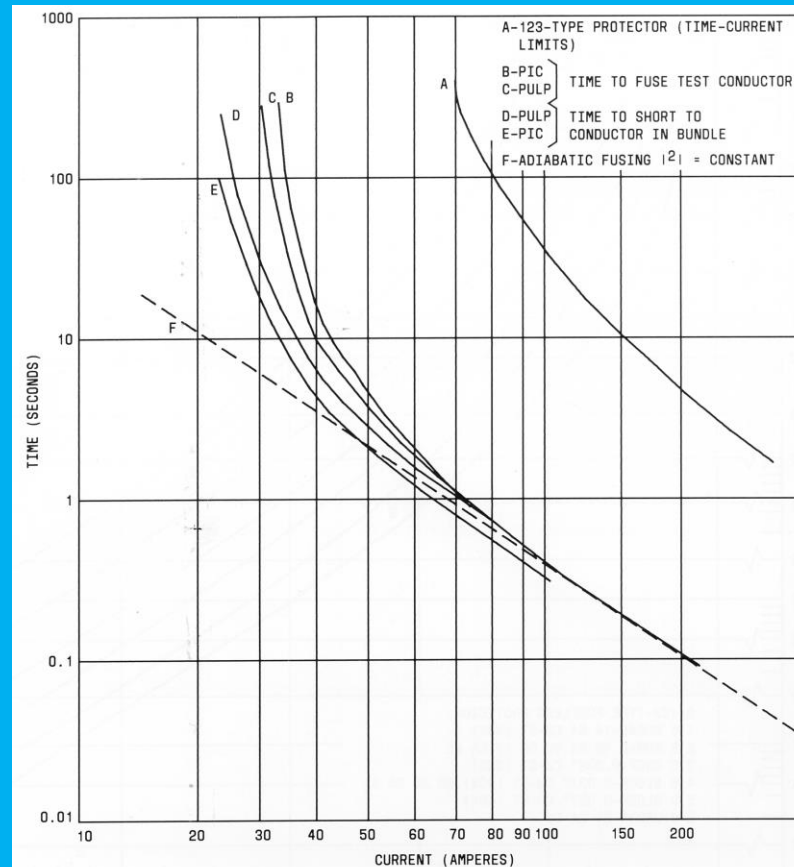


Fig. 15.30—Protective Characteristics of 24-Gauge Copper Cable and the Safe Time-Current Capability of 123-Type Fuseless Protector

Closing Remarks

- All simulations are based on an i^2t limitation for adiabatic times and a fixed current value for thermal equilibrium times.
- The derivation of Northern American simulation curves are based on testing.
- Simulation curves based on insulation temperature rise are more conservative. Example, 26 AWG has a North American fixed current limit of 2.2 A, but in IEC safety standards it is 1.3 A.