Case Studies of Electrical Protection Issues in the Field

DALE STEGMAIER & LARRY PAYNE PEG GENERAL MEETING - 2013







MEASURE SHEATH CURRENT On Cable 17

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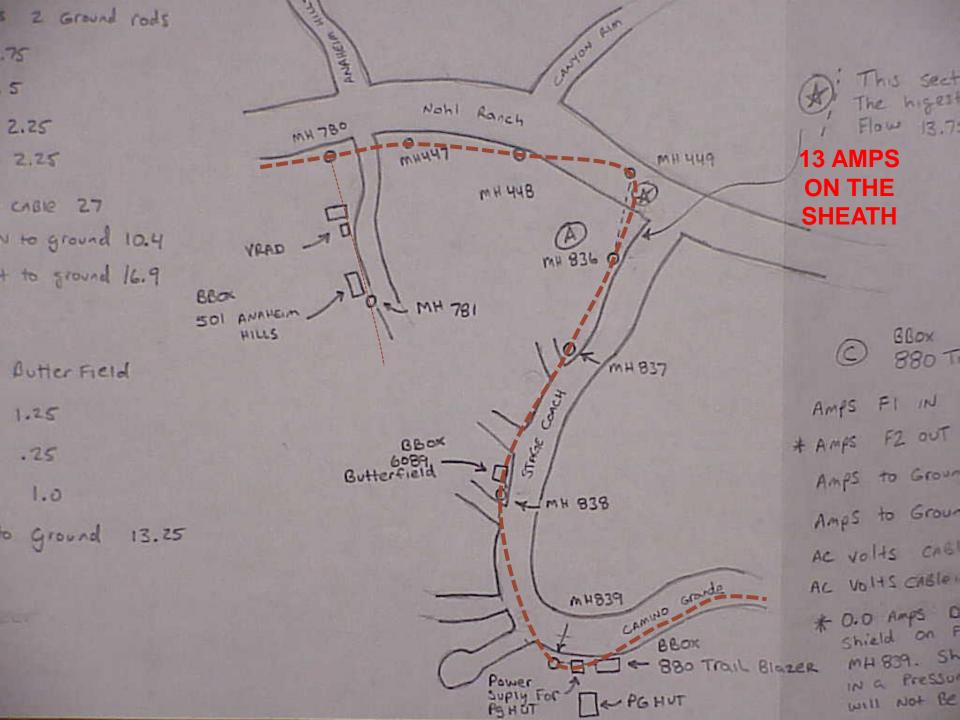
MANHOLE GROUND ROD

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SHIEATCH CURRENT

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21 States

- 1. Cable must have a continuous shield
- 2. Bonds to the MGN and at both ends
- 3. Normally carry from 500 mA to 5000 mA

California

- A. No bonds to MGN
- **B.** Cable bond to ground bed every 1/4 mile
- C. Normally carry from 50 mA to 5000 mA

Readings less than 50 mA indicates an open shield Readings more than 7000 mA *suggest* power system issues

PI (Power Influence) 80 – 90 dBrnC is Marginal PI over 100 dBrnC *suggest* power system issues Noise = Less than 20 dBrnC

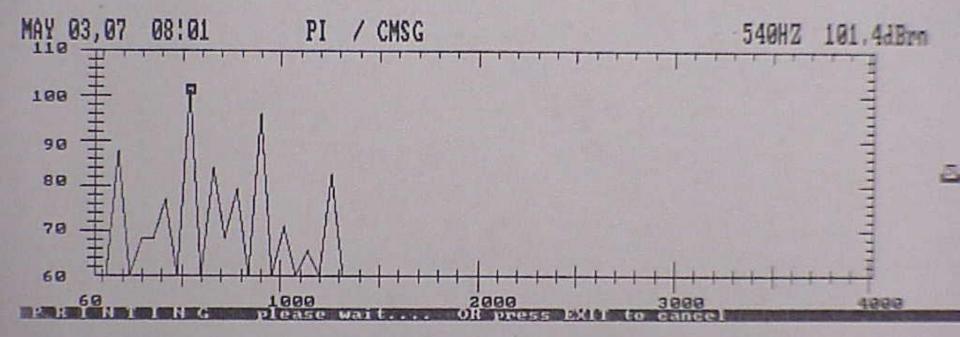
Location	Date		Current	Loss	Noise dBrn		Power Influence		T-R Voltage	Dominant
	5/3/07		mA (21)	dBM (8.5)	Cmsg <20	Flat	Cmsg <85	Flat	AC Volts	Frequency
880 BOX 880 Trail Bloger	Cable 17 Pair 416 BP 416	Dynatel	26.8	5.9	30	100	7100	2.4	T-R -	PLOTI
		Wilcom 132EZ	600 Termination Bridge					R-I	R-G 1675V T-G 16.75V	PG73 PG73
B Box 501 anaberin Hills	Cable 17	Dynatel	28.8	4. 9	19		94		T-R &	PLOTY PLOTS
	Pair 551 BP 701	Wilcom 132EZ	600 Termi Bridge	nation			54042 90		R-G 2.0 T-G 2.0	
	Cable /7	Dynatel	28.9	5.0	30		95		T-R 🗢	PLOTO
	Pair 501 BP 201	Wilcom 132EZ	600 Termination Bridge				540 42 91		R-G 2.0 T-G 2.0	Pco 77
	Cable	Dynatel							T-R	
	Pair	Wilcom 132EZ	600 Termination Bridge						R-G T-G	
	Cable	Dynatel							T-R	
	Pair	Wilcom 132EZ	600 Termination Bridge						R-G T-G	
	Cable	Dynatel							T-R	
	Pair	Wilcom 132EZ	600 Term Bridge	ination			16.20		R-G T-G	

880 trail Blager



PLOT 1

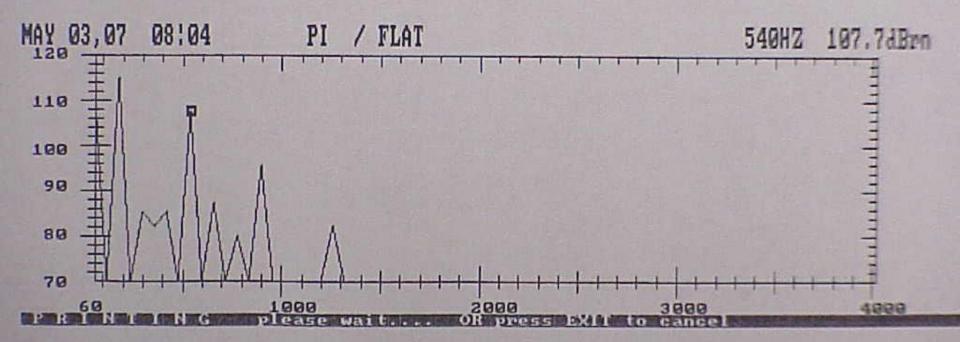
all 17 Pai 416



Flat

PLOTZ

Call 17 Pais 416











State 1







Bond To Ground Ring 6



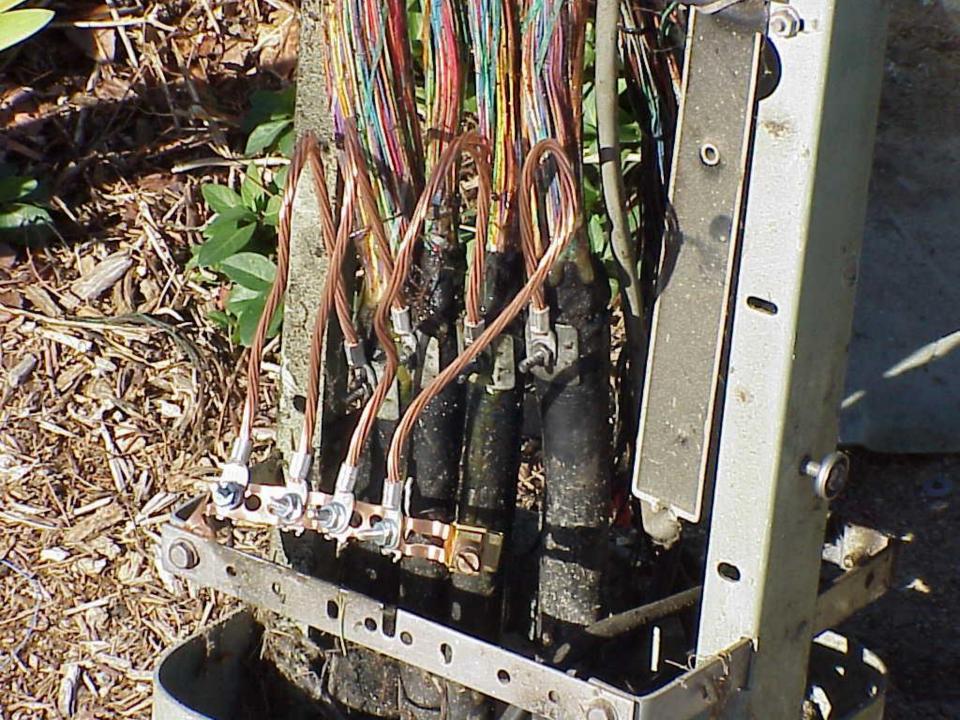












Back To Box 880

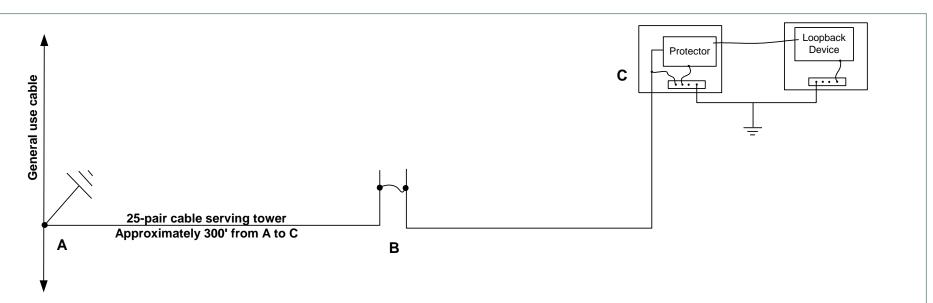
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By clamping on the bond strap at location C and seeing no current flow, I was able to immediately determine the shield wasn't working properly from the ground at point A to the ground at point C. Since this is a 300' section of 25-pair cable, the resistance in the shield between point A and C should be less than 1 ohm (1000' of 25-pair cable has a shield resistance of about 1 ohm).

I then removed the bond at point C and measured the induced voltage which was 0.1 volts. This indicted the shield wasn't completely open, so I re-attached the bond and used a more sensitive clamp-on ammeter (AEMC 3731) and measured 0.007 amps. This allowed me to do the simple calculation of (V = I X R) and determine how much resistance I had in this 300' section of shield. My resistance was R = (0.1 / 0.007) = 14 ohms. Therefore, we had a high resistive splice that was adding this additional resistance and was drastically limiting the amount of current that could flow in the shield.

The bonds in the pedestal at location B was where the problem existed. When this bond was replaced, the resistance dropped from 14 ohms to less than 1 ohm and the current increased from 0.007 amps to 1.12 amps.

This section now has 1.12 amps of current flowing on the shield (99% more than before). This increased current is now creating a strong enough magnetic field around the cable to effectively cancel the magnetic fields from the power lines and we can now ground our loopback without the circuit taking errors. When we only had 0.007 amps current flowing in the shield, the magnetic field it was creating around our cable was cancelling less than 1% of the induction from the power lines and thus enough voltage existed on the pairs between the pair and earth that everytime we grounded the loopback, the induced voltage was enough to allow the protectors in the loopback card to intermittently fire to earth and thus caused continued intermittent errors on the circuit.





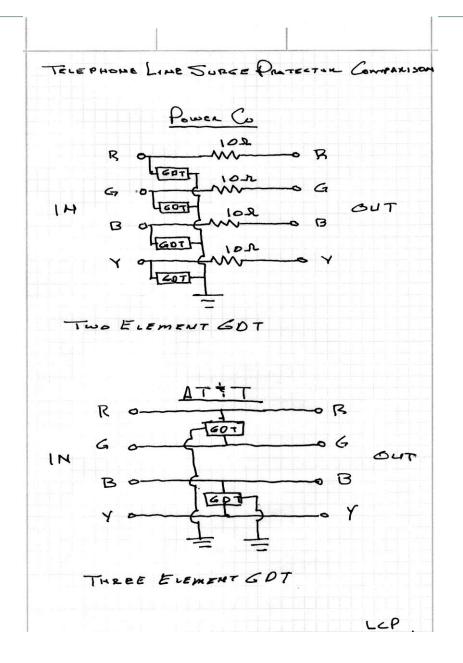


"Special Protector"

- Required by Power Company for Warranted Protection from Damage
- Placing in series and on customer side of telephone protector
- Would not pass HPNA Signal
- NEC issues
- No listing mark

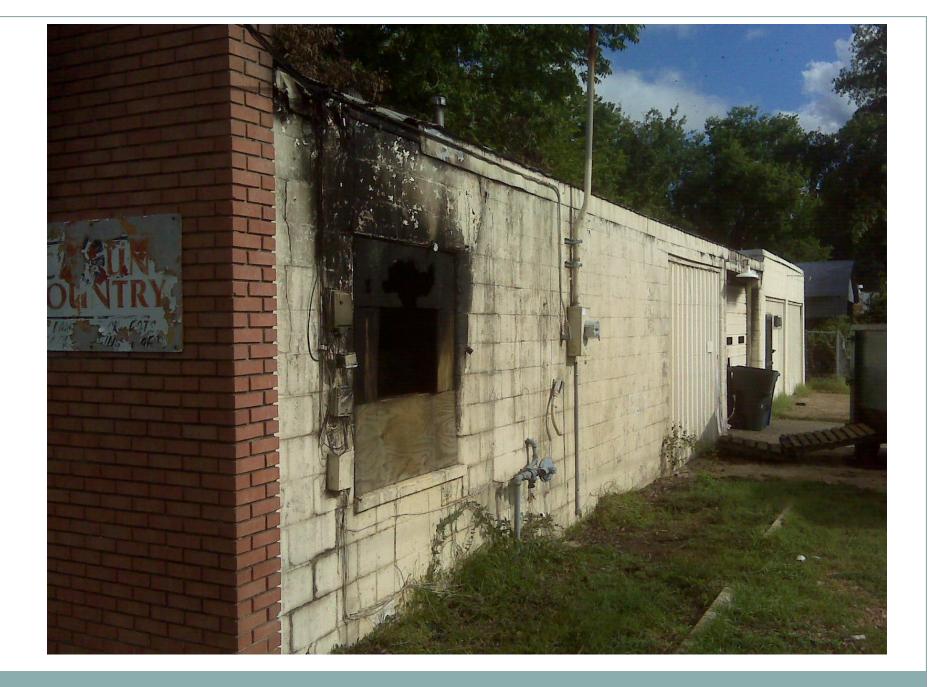






Design Question

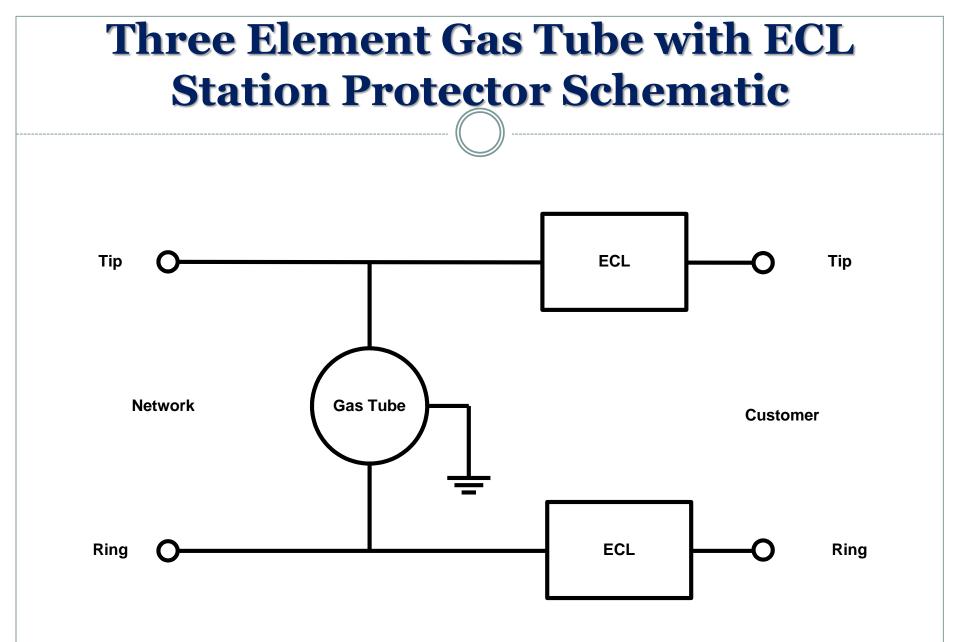
- 10 Ohm provides coordination, but not calculated
- Two element gas tubes
 - A device for each conductor
 - Longitudinal to Metallic Conversion during a surge
- Three Element Gas Tube
 - No Longitudinal to Metallic Conversion during a surge





Electric Fence Controller Damage

- Controller for electric fence being damaged frequently by lightning storms.
- Suggested use of special protector
- Originally designed for telecommunications equipment at customer premise.
- GDT and ECL



ECL / Gas Tube Function

- Switches very quickly from a low resistance state approximately 12 Ω to an open circuit when current threshold is exceeded
- Signal / surge path is opened until gas tube fires
- Signal / surge path is shorted to ground until surge is removed
- Lightning results no more damage to electric fence controller

Alternative and Creative Use of an RT Site

TRUE...





