



Level of confidentiality: PUBLIC



GROUNDING AND BONDING

An overview of recent success stories

James Crook, Eng.
Standards and Engineering Support



Biography: James Crook, Eng.



- **1985:** Graduate of the Joncquière Technical College (Electronics)
- **1989:** Graduate of the Université du Québec à Trois-Rivières (Bachelor of Electrical Engineering)
- **1990:** Professional Field Engineer for Captel (Turnkey microwave and fibre-optic integration project)
- **1992:** Joined Hydro-Québec (Telephony expert in generating stations and substations)
- **1998:** Joined Intrawest – Mont Tremblant Resort (Telecom project management & expertise)
- **2001:** Established a professional engineering firm – Consulting work for Hydro-Québec & Intrawest (Telecom infrastructure, project expertise & operations)
- **2009:** Returned to Hydro-Québec (Technical expertise division, grounding and protection)
- **2011:** Transferred to Standards and Engineering Support

Today's Agenda

Objective: Present some of the more recent best practices used in telecommunication grounding and bonding at Hydro-Québec.

Three parts:

 Why worry about grounding?

 Where are the risks?

 How grounding models compare?



Why worry about grounding?

General issues

- Our technical problems
 - Propagation of impulse noise
 - Unexplained service downtime/interruption
 - Deficient immunization against power faults (SPDs)
 - Insufficient fault energy dissipation (lightning protection)
 - Doubtful grounding practices (among professionals)
 - Lack of standards for hardware and installation techniques (among contractors)



10-002 Object

(1) The object of bonding metal parts and metal systems together and to the grounded system conductor is **to reduce the danger of electric shock or property damage** by providing a low impedance path for fault current back to the source and to establish an equipotential plane such that the possibility of a potential difference between metal parts is minimized.

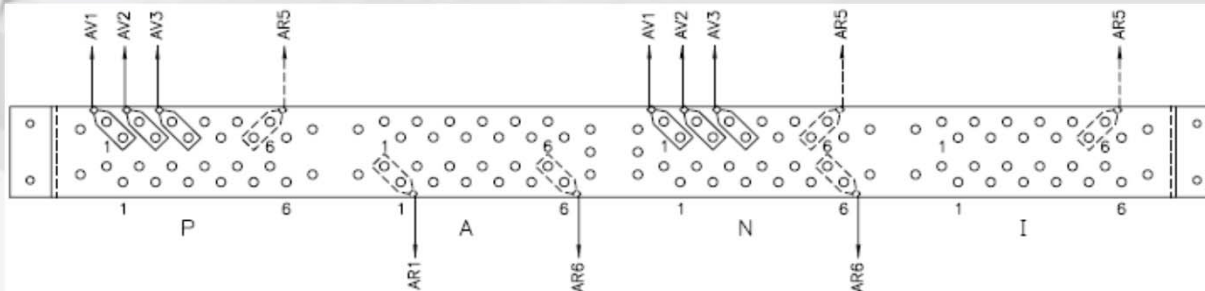
(2) The object of grounding the electrical system and non-current-carrying metal parts is **to connect the earth to the equipotential plane**, thereby minimizing any potential difference to earth.

(3) The object of using an ungrounded system or a system incorporating neutral grounding devices **is to provide an alternative to a solidly grounded system**, thereby limiting the magnitude of fault current and minimizing the damage resulting from a single fault.

Why worry about grounding?

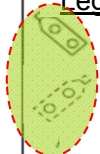
General philosophies(MTGB)

T1.313-2003



P	A	N	I
1 - Week			
Current line radio	Outside building ground (peripheral, web)	DC power plant (return bar)	DC Level I equipment frame or cabinet
Gas tube protector	Main building ground (water pipe)	Equipment grid	DC Level II (switches and routers)
Metallic conduits (ingress/egress)	Main building ground (electrical, structural)	DC converter (return bar)	DC Level III (routers)
	Secondary telecom room	DC equipment frame or cabinet (general)	
		DC PABX	
2 - Medium			
Metallic sheath cables box			
AC distribution panel box			
Fire alarm box			
AC equipment box			
Heating unit			
Air conditioning unit			
Out plant cables			
Electric motors			
Cable dispatching frame			
PAGA system			
AC frame or cabinet (routers and/or switches)			
3 - Strong			
Antistatic floor (local)			
Raised floor (local)			
UPS system			
Inverter			
Generator			
Tower obstacle lights			

Legend:



Lug termination on front
Lug termination on back

NOTE: angled hole array allows to add or remove lugs while maintaining lug contact on opposite side of MTGB

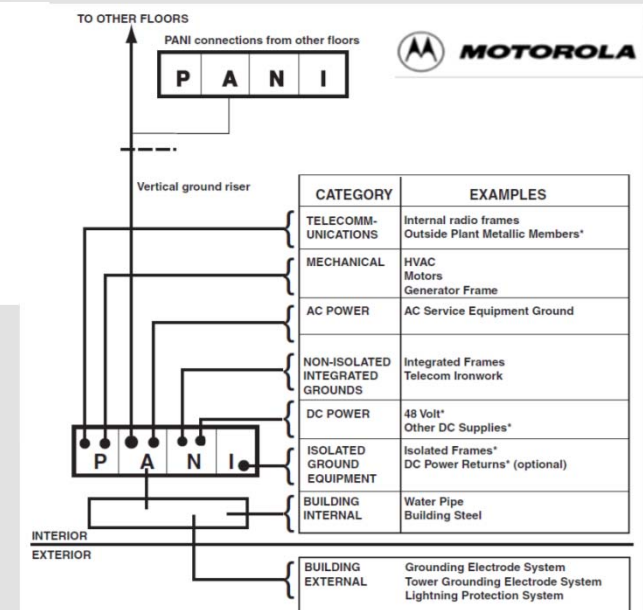


FIGURE 5-23 PANI GROUNDING SYSTEM SEQUENCE

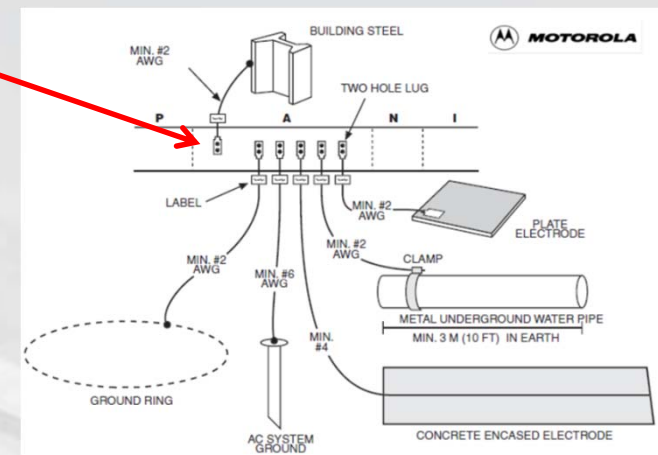


FIGURE 5-10 TYPES OF ACCEPTABLE GROUNDING ELECTRODE SYSTEMS

Why worry about grounding?

General hardware (torque efficiency)

Boulon (diamètre)			INSTALLATION		MAINTENANCE	
(po)	(/ 64po)	(mm)	N-m	lb-pce	N-m	lb-pce
1/8	8	3,2	2,3	20	2,0	18,0
9/64	9	3,6	2,8	25	2,5	22,5
5/32	10	4,0	3,4	30	3,1	27,0
11/64	11	4,4	4,0	35	3,6	31,5
3/16 #10	12	4,8	4,5	40	4,1	36,0
13/64	13	5,2	5,1	45	4,6	40,5
7/32	14	5,6	6,2	55	5,6	49,5
15/64	15	6,0	7,3	65	6,6	58,5
1/4	16	6,4	7,9	70	7,1	63,0
5/16	20	7,9	12,4	110	11,2	99,0
3/8	24	9,5	18,1	160	16,3	144,0
7/16	28	11,1	24,9	220	22,4	198,0
1/2	32	12,7	31,6	280	28,5	252,0

Copper (bronze-silica)



Nuts & bolts assembly

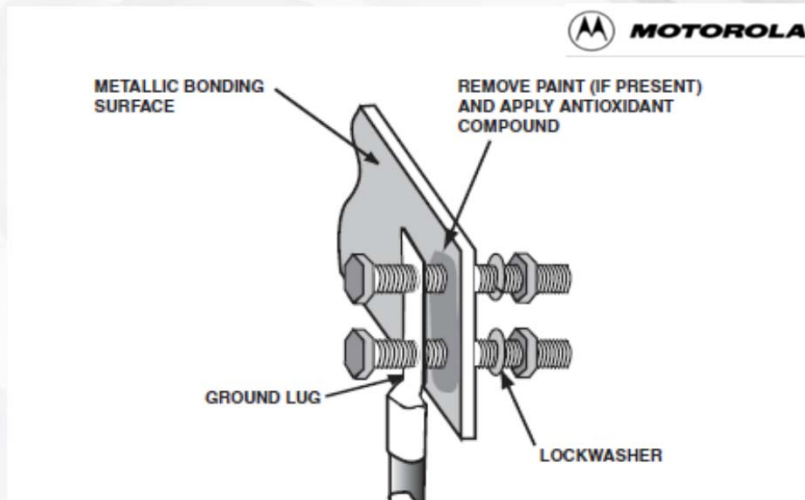
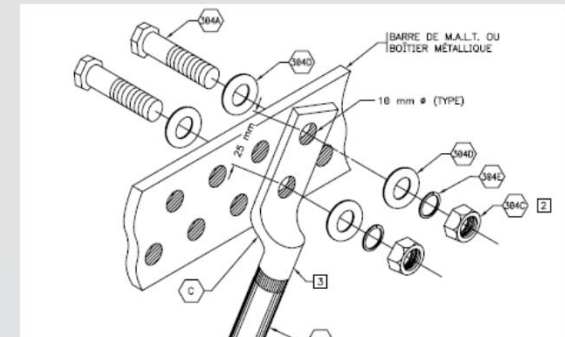
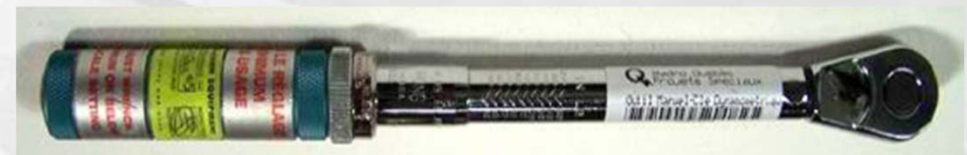
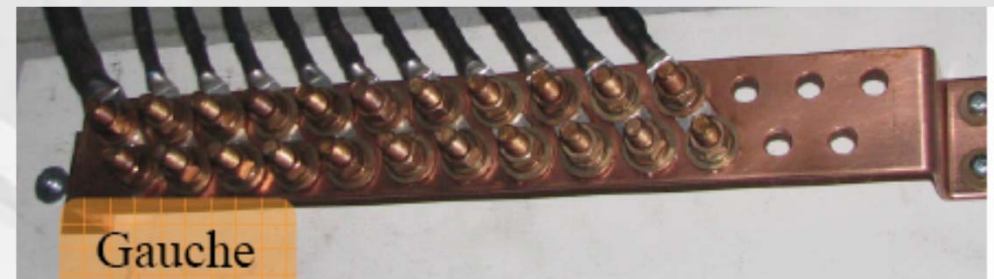


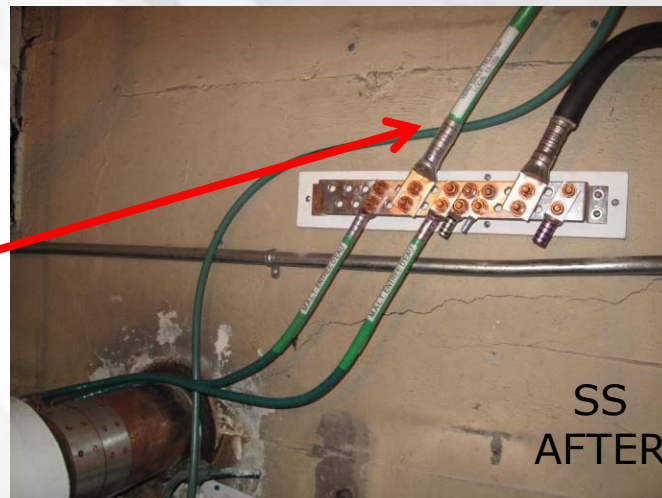
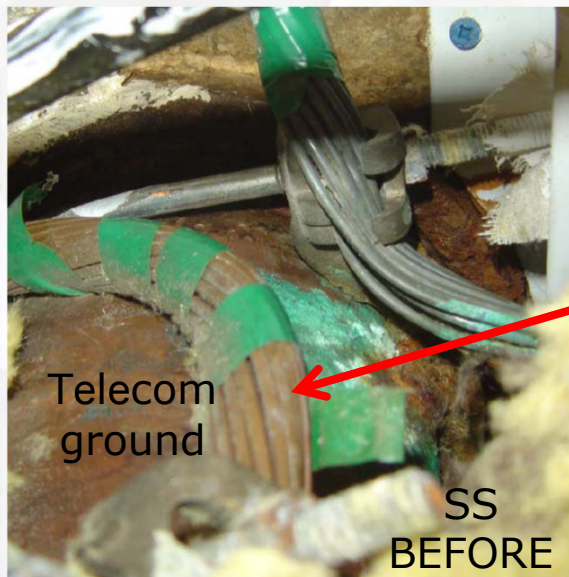
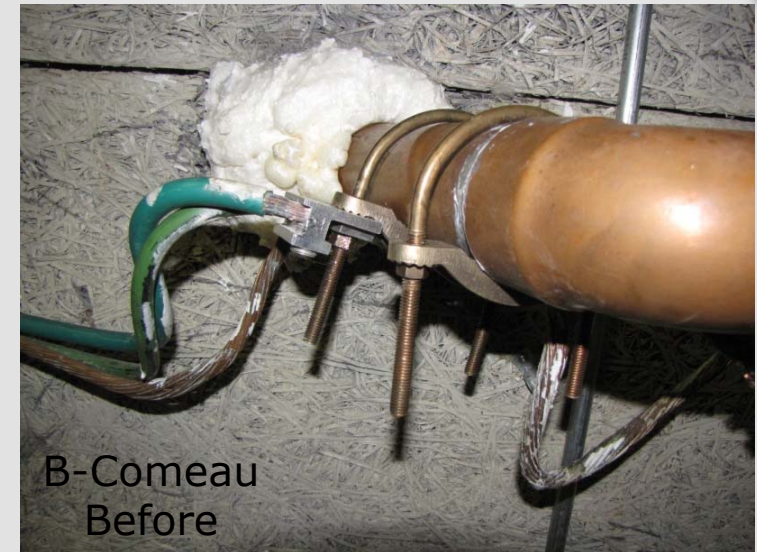
FIGURE 5-19 PROPER LOCATION OF WASHER WHEN CONNECTING GROUND LUG



Why worry about grounding?

General improvement

Quality of building ground



Where are the risks?

Grounding: Electric vs telecom

IEEE Std 1692™-2011
IEEE Guide for the Protection of Communication Installations from Lightning Effects

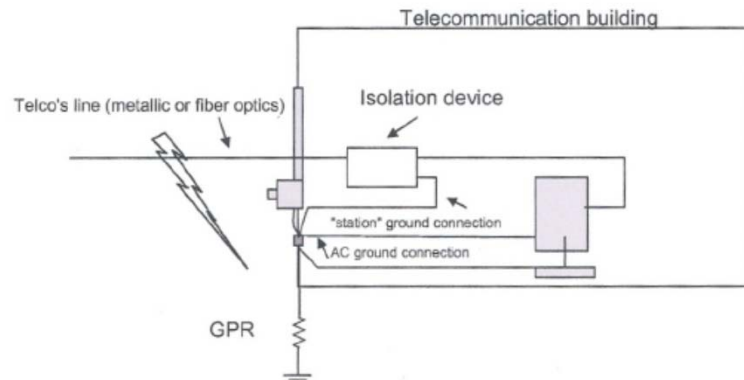
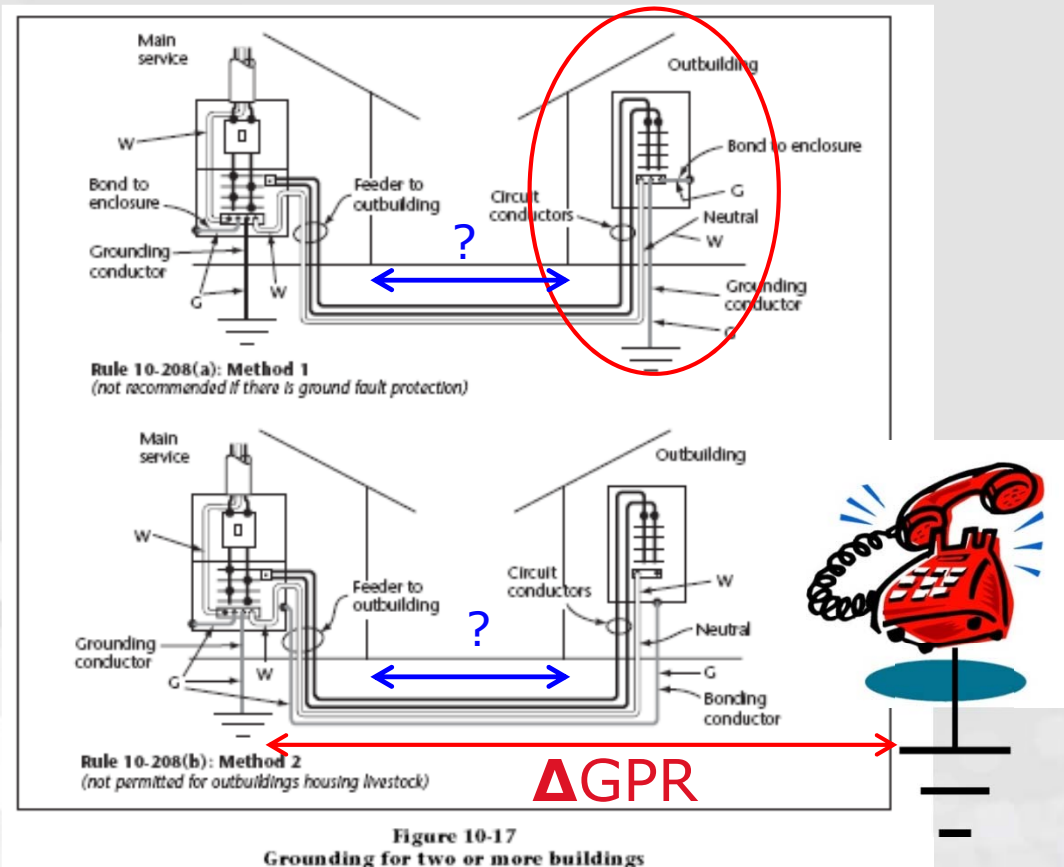


Figure 3—Example of an acceptable and proper installation. Power, equipment, and protection device grounds are at the same reference.

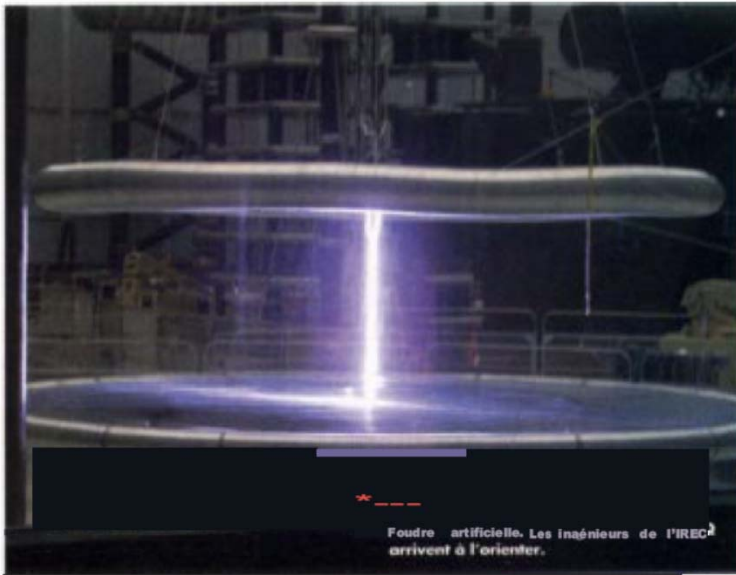
10-208 Grounding connections for two or more buildings or structures supplied from a single service

Where two or more buildings or structures are supplied from a single service,
(a) the grounded circuit conductor at each of the buildings or structures shall be connected to a grounding electrode and bonded to the non-current-carrying metal parts of the electrical equipment; or
(b) except for buildings housing livestock, the non-current-carrying metal parts of the electrical equipment in or on the building or structure **shall be permitted to be bonded to ground by a bonding conductor run with the feeder or branch circuit conductors.**

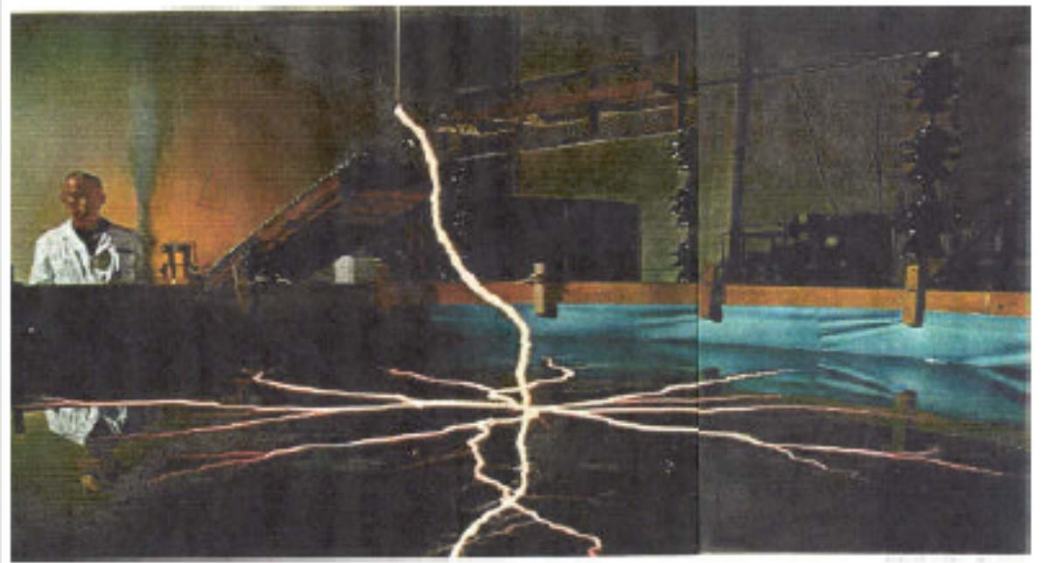


Where are the risks?

Our concern: Lightning



Québec-Science / Février 1999 23



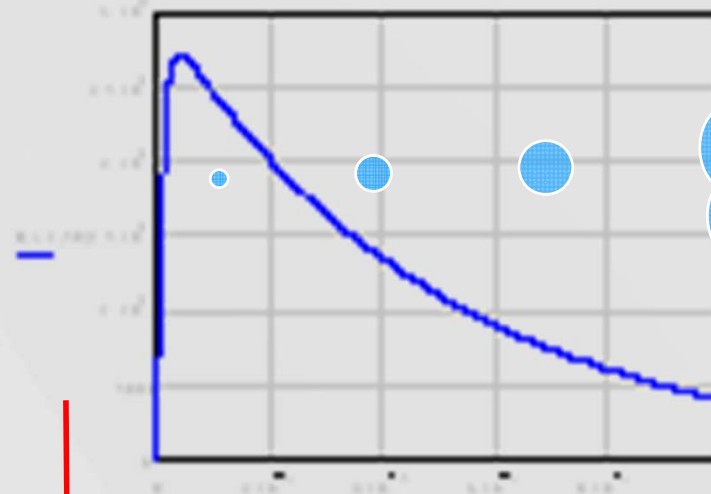
(This photograph appeared in the August, 1969 issue of The National Geographic Magazine.)



Lightning strikes at Lake Macquarie, Peter Kenelly

Where are the risks?

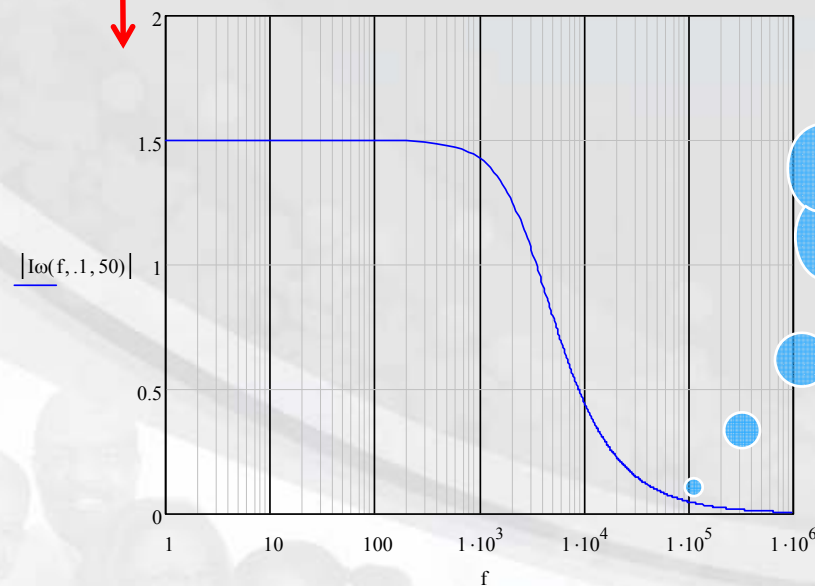
Voltage dissipation below 100 kHz



di/dt can cause arc flashes and dielectric breakdown

Current vs time

Fourier transformation



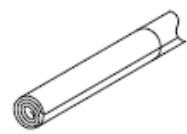
Grounding configuration must be efficient up to 100 kHz.

Frequency vs time

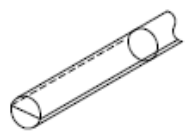
Equipotentiality at lower frequencies

Where are the risks?

Ground configurations



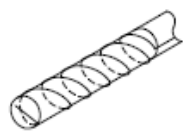
□
CONFIGURATION 1
SPIRALE STANDARD
POTEAU



□
CONFIGURATION 2
4 MÉNÉS DE CONDUCTEUR
POTEAU



□
CONFIGURATION 3
8 MÉNÉS DE CONDUCTEUR
POTEAU



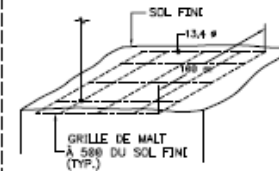
□
CONFIGURATION 4
10 MÉNÉS DE CONDUCTEUR
(5 TOURS COMPLETS)
POTEAU



□
CONFIGURATION 5
6 MÉNÉS DE CONDUCTEUR
POTEAU



CONFIGURATION 6
POINTE DE TERRE ENTRE (2) PIQUETS
(VUE EN PLAN)



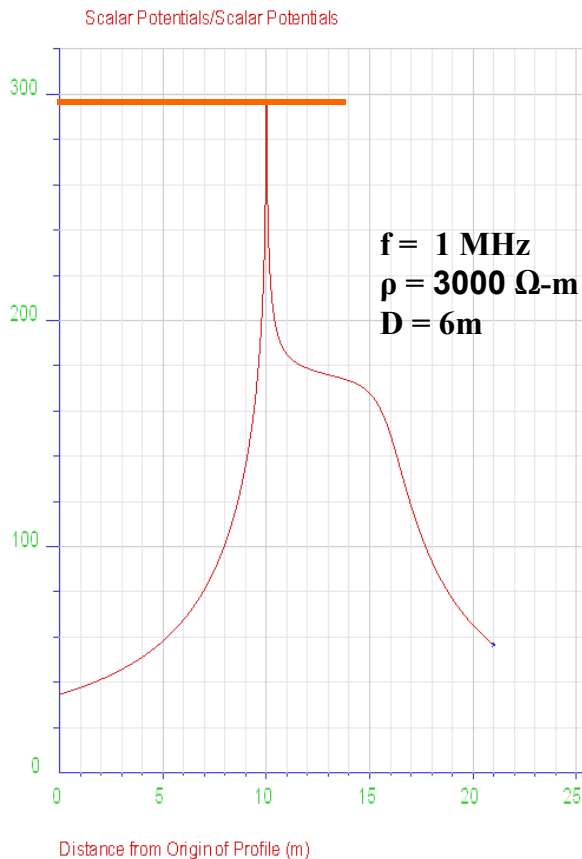
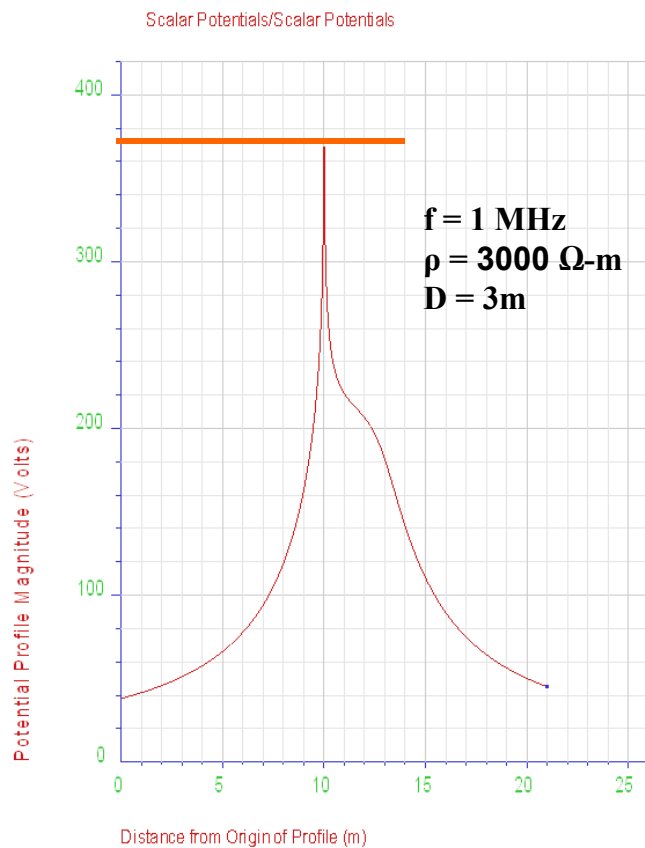
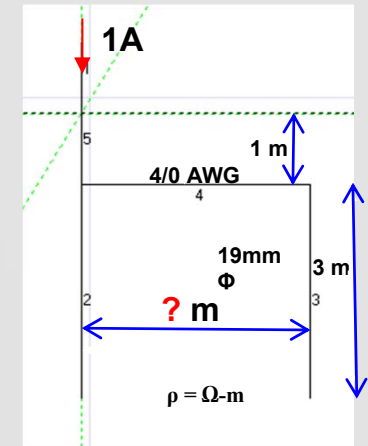
CONFIGURATION 7
GRILLE DE TERRE (TYP.)

Where are the risks?

Models : 2 rod electrodes

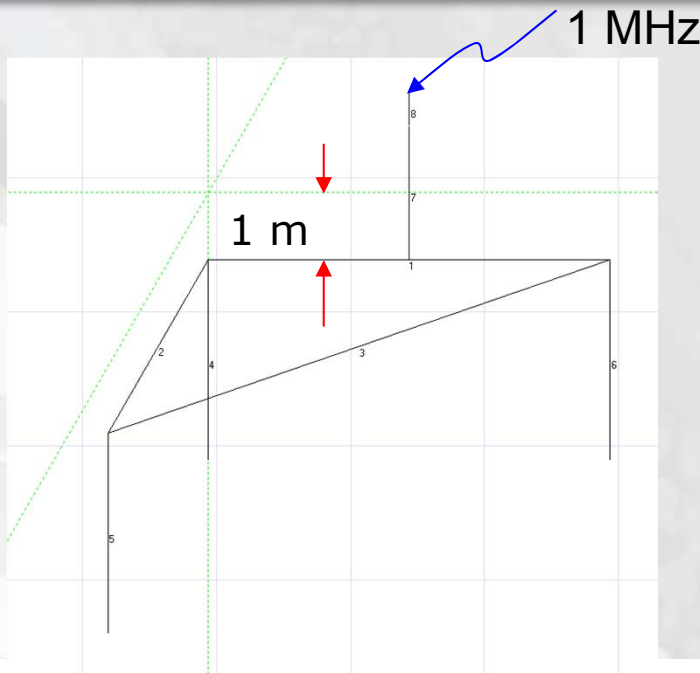
10-700 Grounding electrodes (see Appendix B)

- (1) Grounding electrodes shall consist of
 - (a) manufactured grounding electrodes;
 - (b) field-assembled grounding electrodes installed in accordance with this Rule; or
 - (c) in-situ grounding electrodes forming part of existing infrastructure as defined in this Rule.
- (2) Manufactured grounding electrodes shall
 - (a) in the case of a rod grounding electrode, consist of **2 rod electrodes** (except for a chemically charged rod electrode where only one need be installed) **spaced no less than 3 m apart**,
 - (i) bonded together with a grounding conductor sized in accordance with Rule 10-812; and
 - (ii) driven to the full length of the rod; or

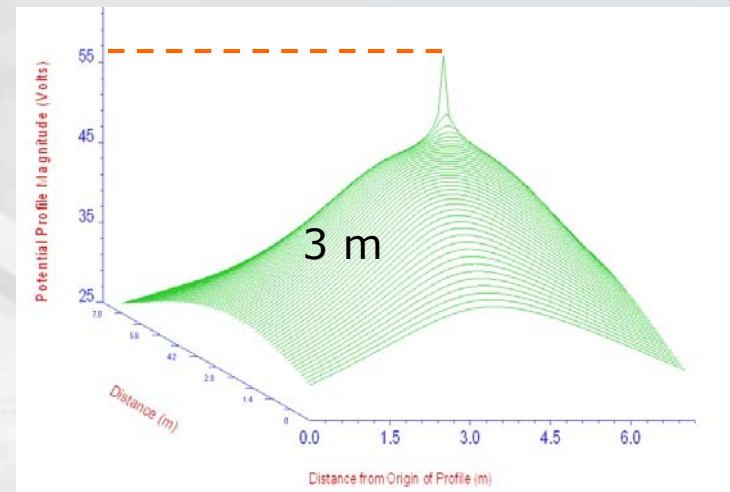
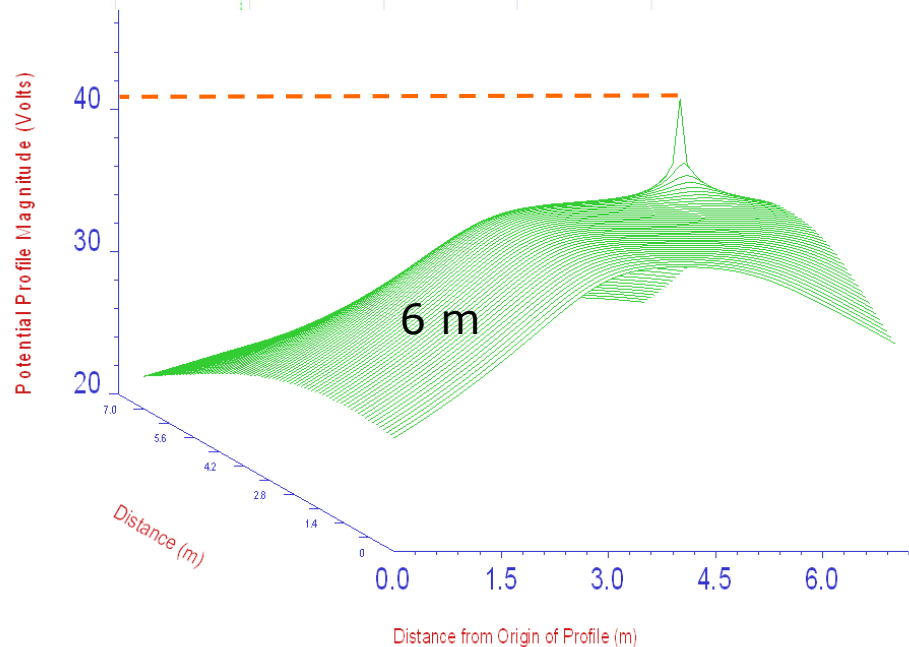
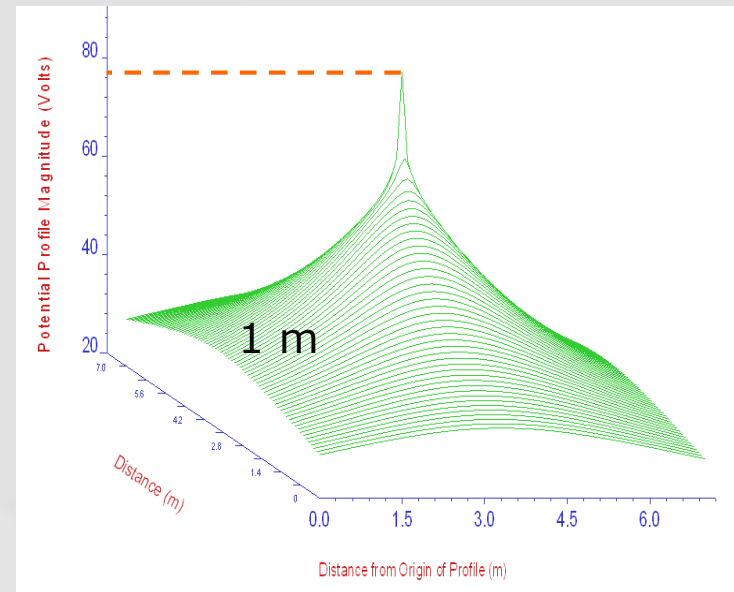


Where are the risks?

Models: Equilateral triangle configuration

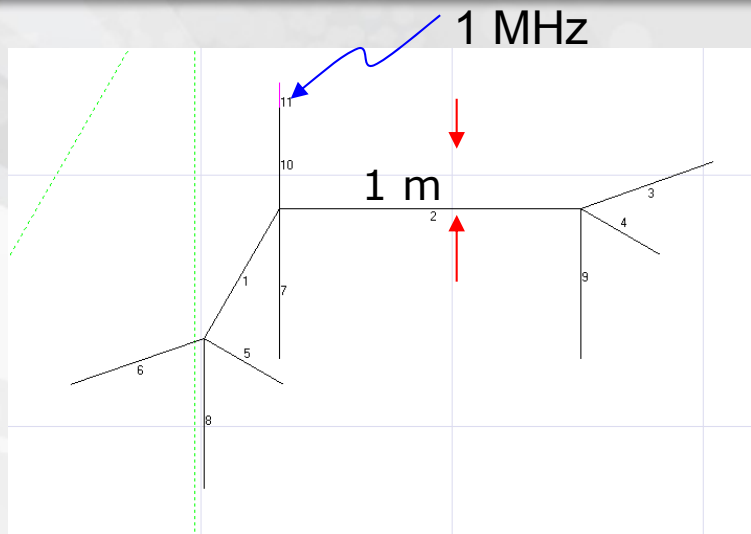


3 m
19 mm Φ
 $\rho = 300/3000 \Omega$



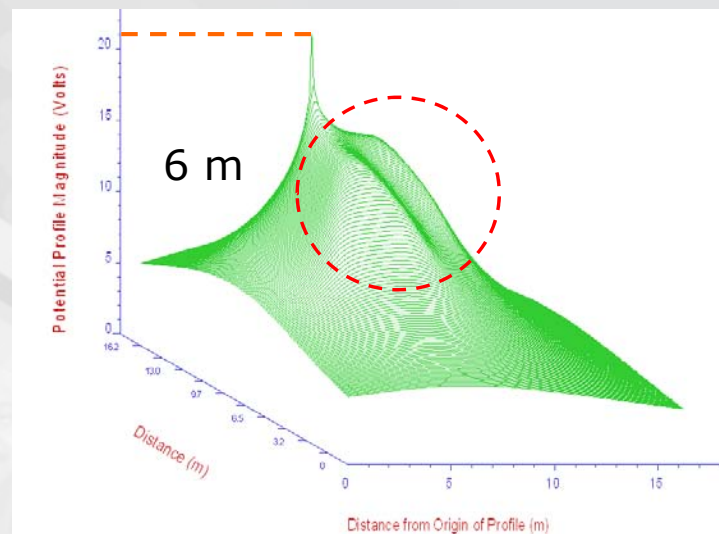
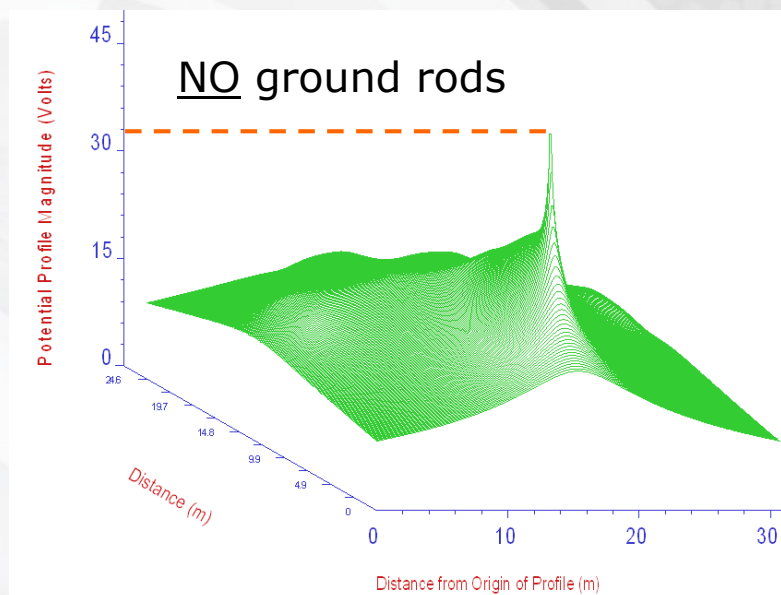
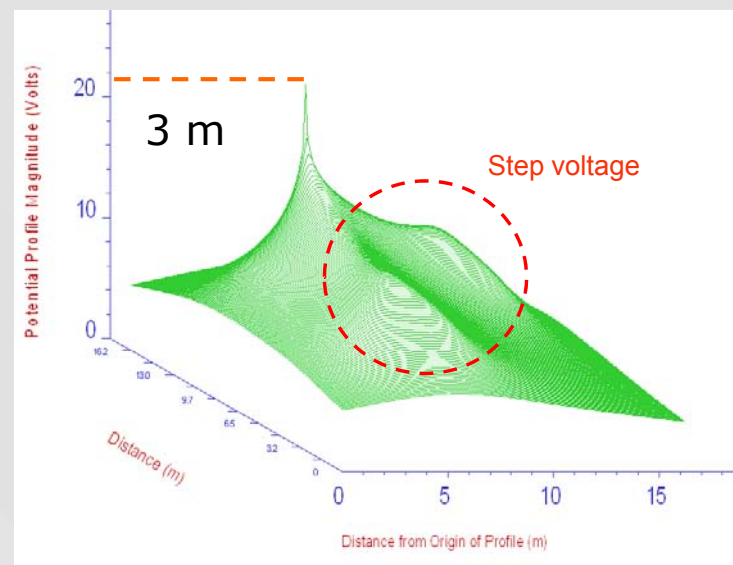
Where are the risks?

Models: Web configuration



3 m
19 mm Φ

$\rho = 300/3000 \Omega$



Where are the risks?

Models: Overall performance Υ vs. Δ

Impulse of 1 X 50 μ s
Frequency domain

Impédance en fonction de la fréquence

Impédance en fonction de la fréquence

Soil a: $\rho = 100 \Omega\text{-m}$

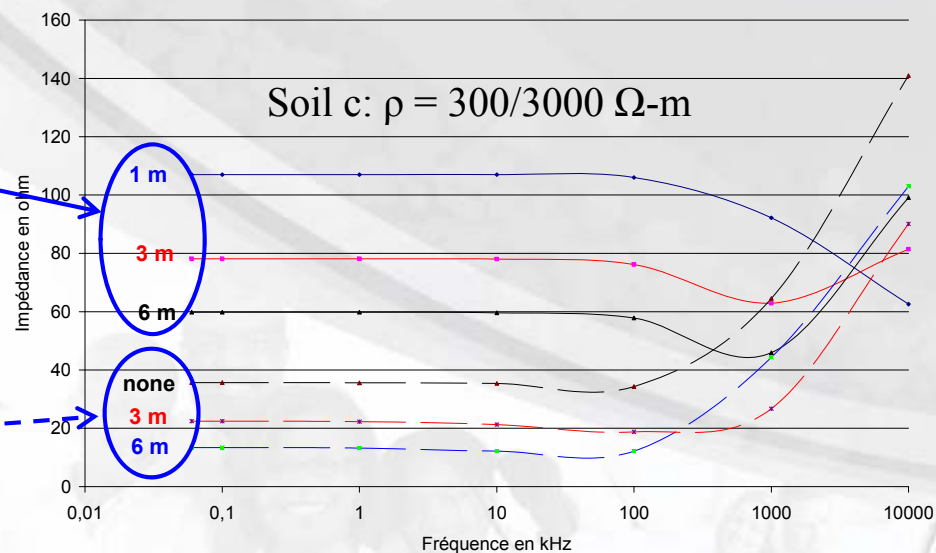
Soil b: $\rho = 100/20 \Omega\text{-m}$

Model 1a/b/C

Model 2a/b/C

Impédance en fonction de la fréquence

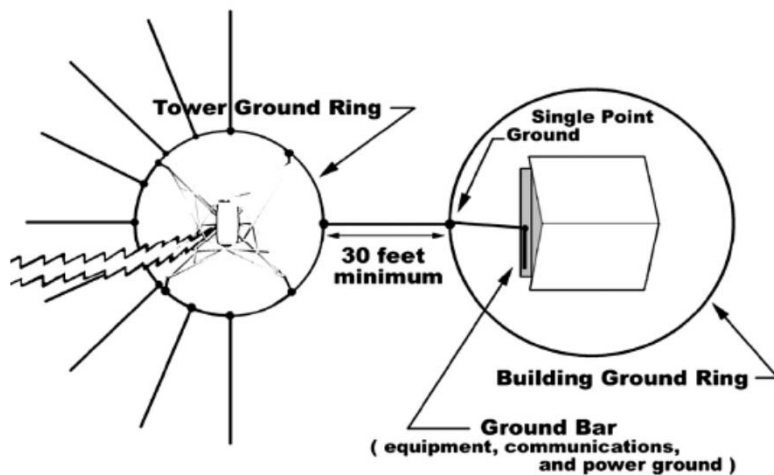
Soil c: $\rho = 300/3000 \Omega\text{-m}$



Where are the risks?

Models: Tower grounding

IEEE Std 1692™-2011
IEEE Guide for the Protection of Communication Installations from Lightning Effects



The ideal number of radial counterpoises recommended is ten (see Block [B5]). The maximum effective length of each radial counterpoise (see Block [B5]) is 24 m (80 feet) each. Longer length radial counterpoises will offer little dissipation improvement because the lightning strike current will not remain on the radial counterpoises for much over 24 m (80 feet).

In sites with limited space (i.e., real estate limitations or restrictions), the recommended grounding system is, at a minimum, 60 m (200 feet) of grounding conductors. This includes a ring ground of 12 m (40 feet) and four radial counterpoises, each 12 m (40 feet) in length.

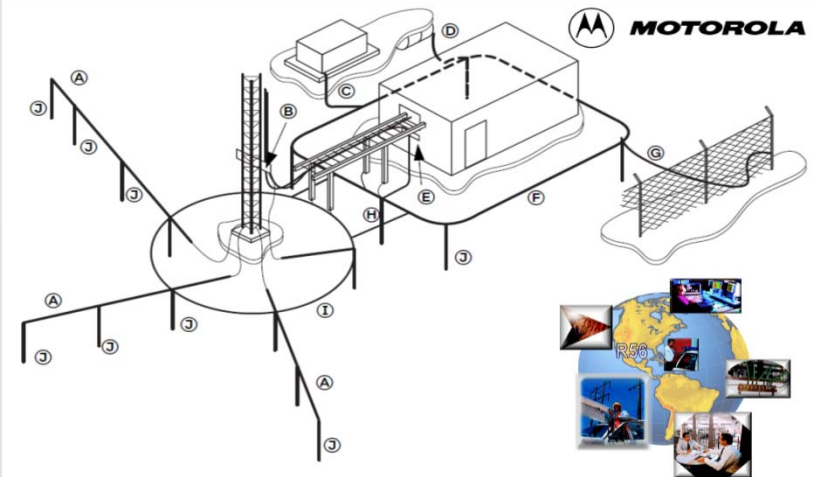
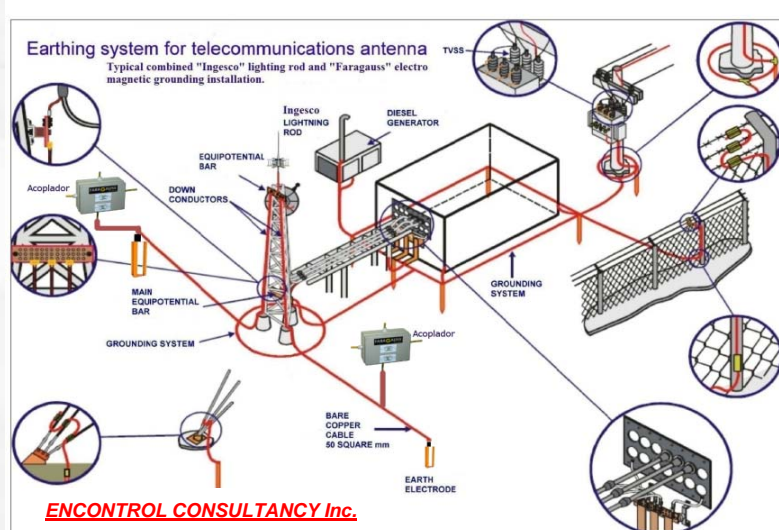


FIGURE 4-4 TYPICAL EXTERNAL GROUNDING ELECTRODE SYSTEM

Standards Committee T1
Telecommunications

T1.313-2003

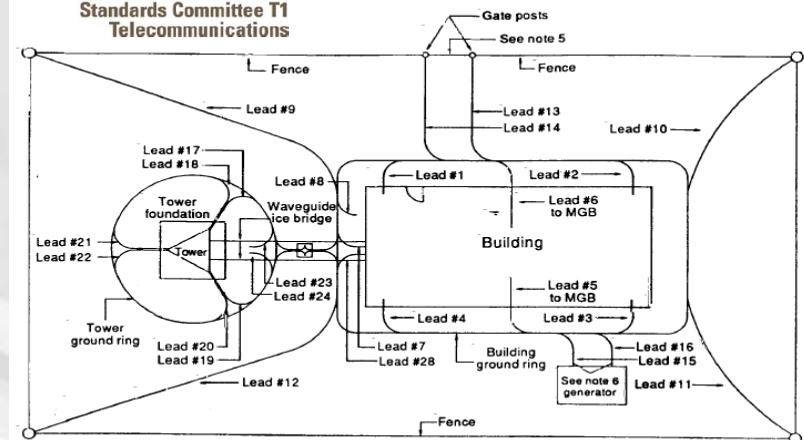
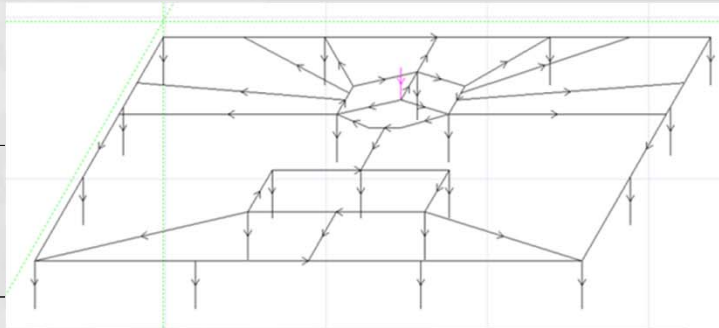
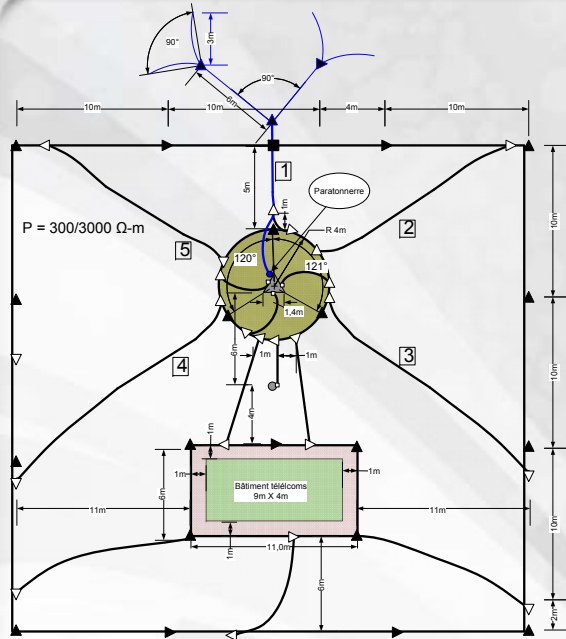


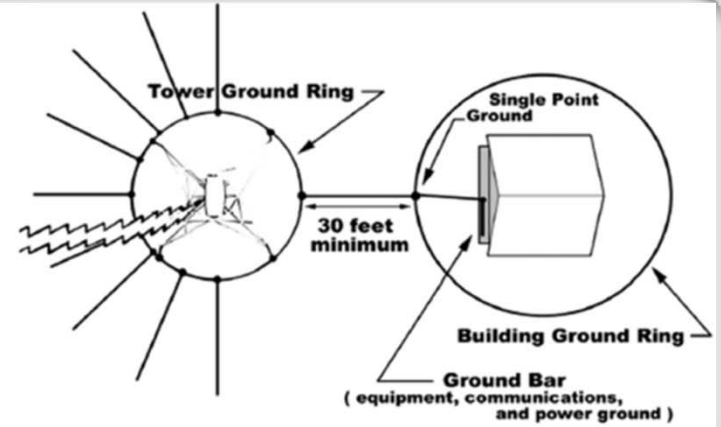
Figure 3(a) - Supplemental radio microwave tower site grounding

Where are the risks?

Models: Tower grounding

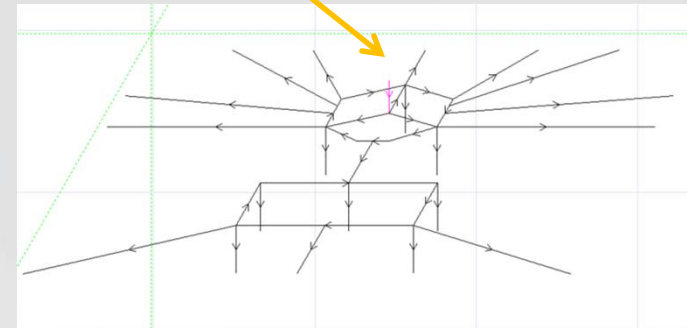
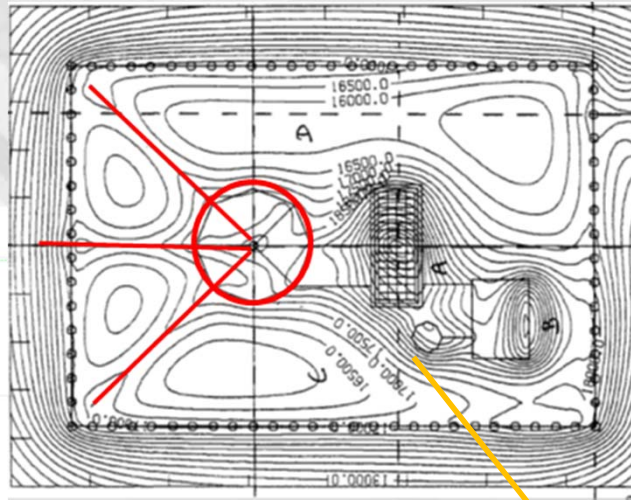


10 radials with a fence GND

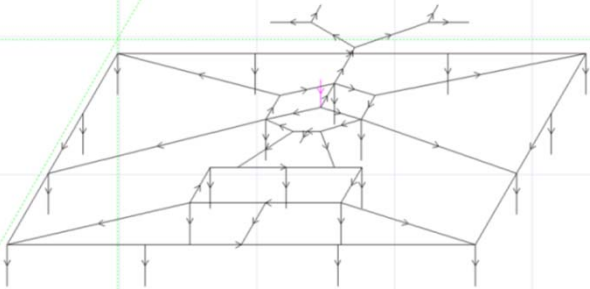


NOTE—Reprinted with permission from Duckworth et al.[B10]

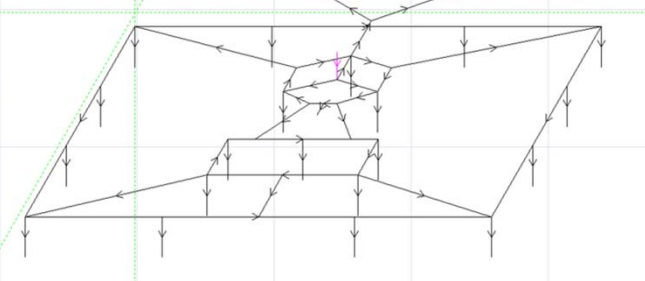
Figure 7—Example of a grounding system



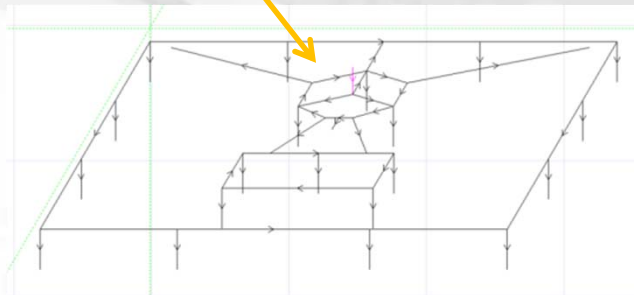
10 radials without a fence GND



5 radials with a fence GND



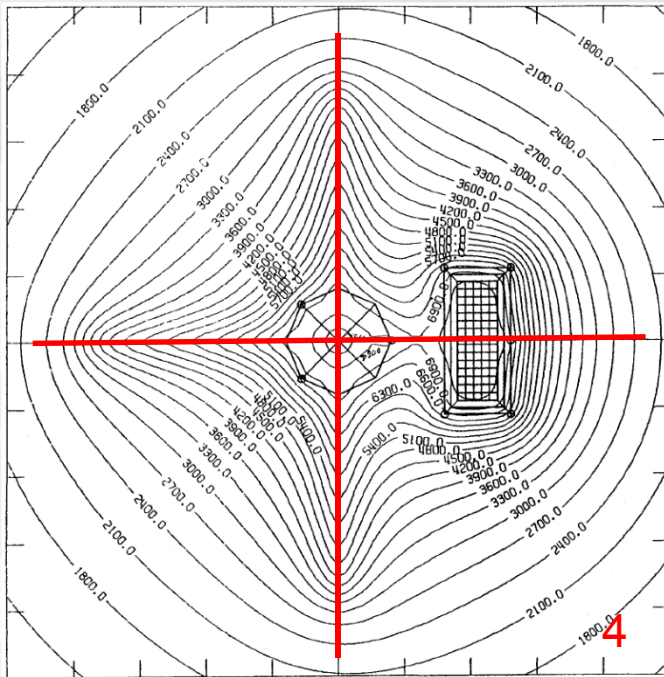
3 radials with a fence GND



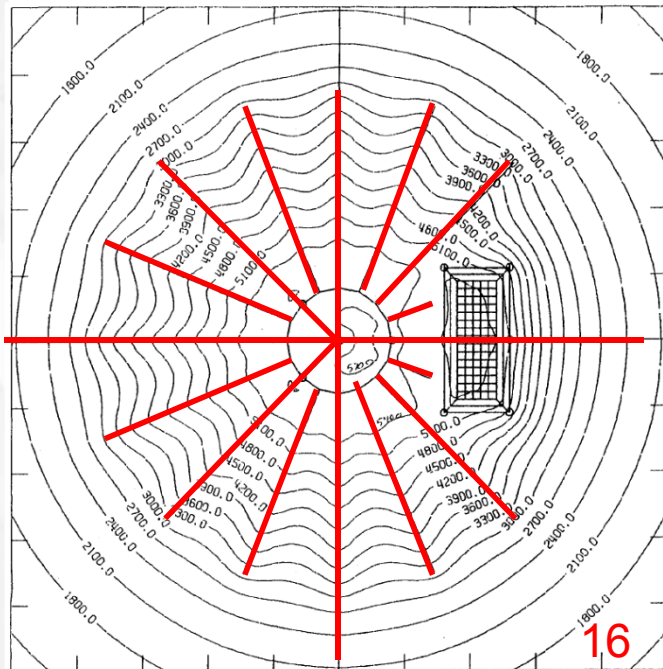
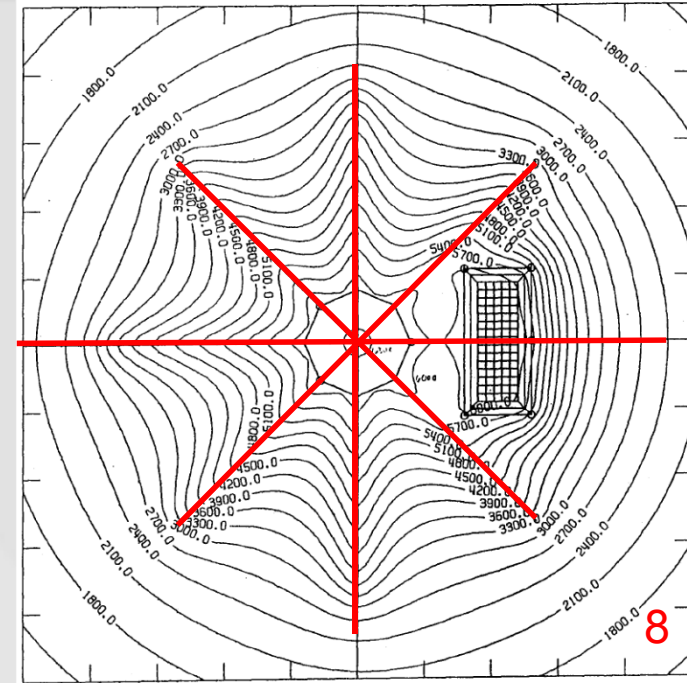
3 radial not connected to the fence GND

How do grounding models compare?

HQ-CG-PT-CEM601-1, 1994



CYMGRD - 1992
 $P = 10 \Omega\text{-m}$
 $F = 60 \text{ Hz}$



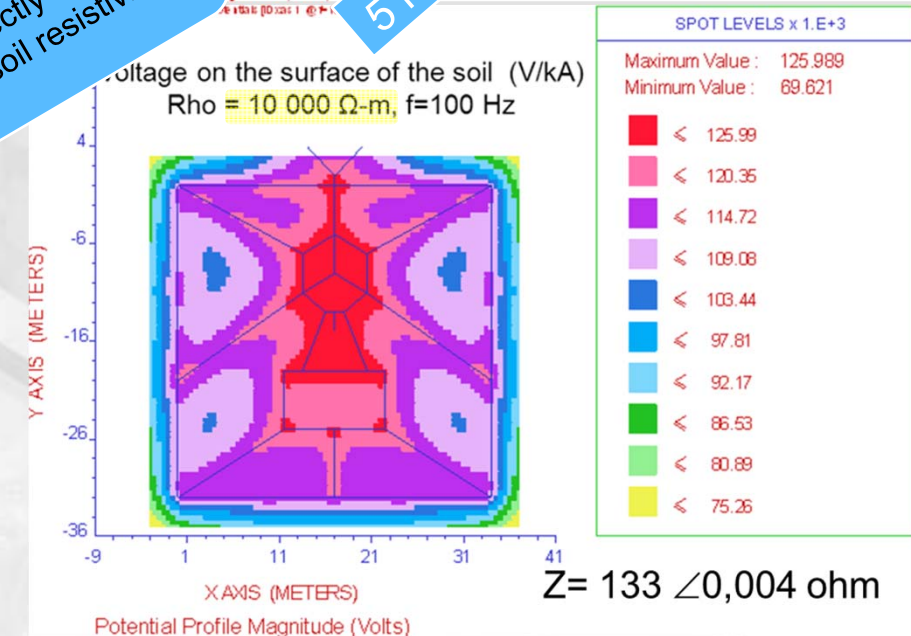
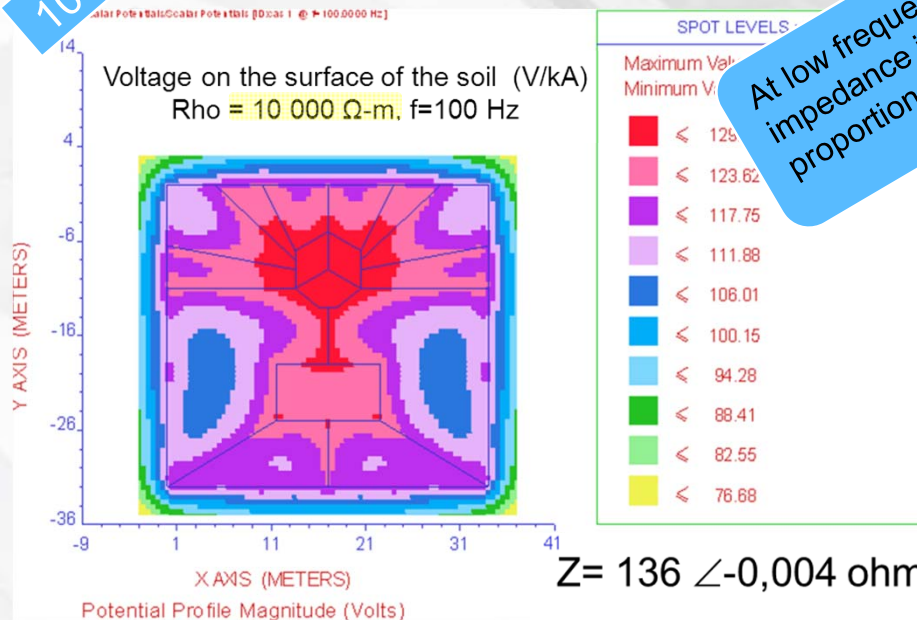
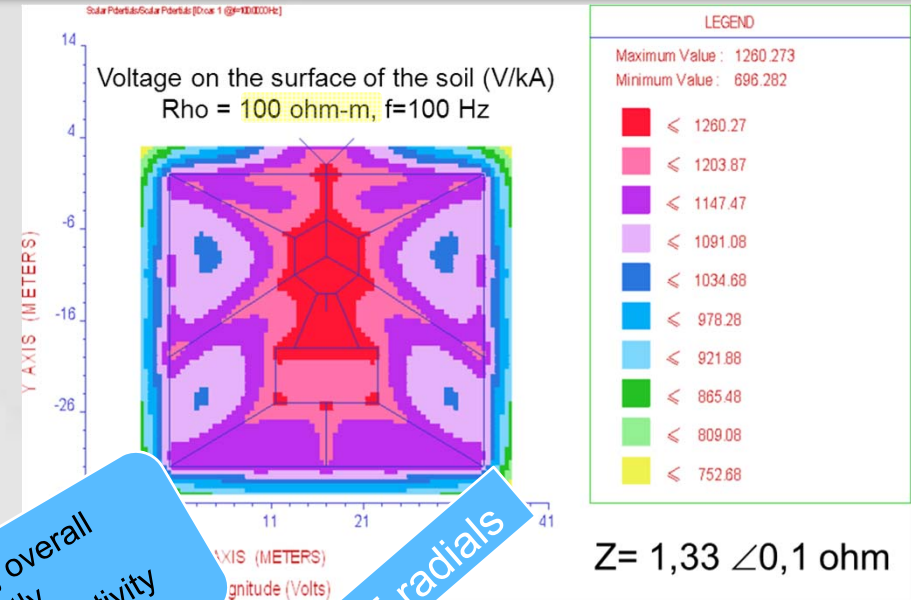
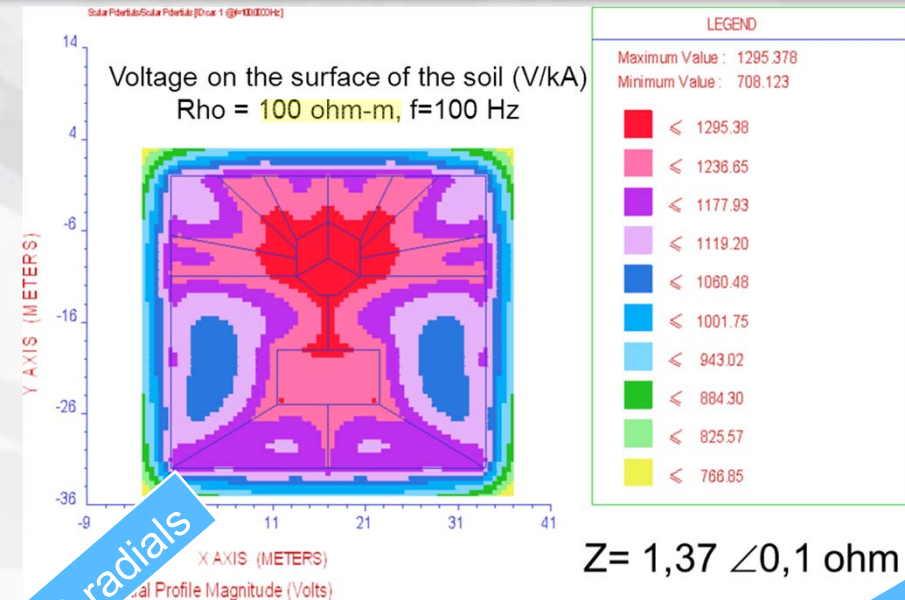
- Uniform step voltage within the tower ground loop
- Increasing number of ground rods above 3 has no significant effect
- Number of radials has no influence on ground potential level
- Increasing the number of radials decreases ΔV in the area (step voltage)
- Adding a 300-mm layer of crushed rock on top of local soil improves touch voltage tolerance values

CG-PT-CEM601-1

MARS 1994

How do grounding models compare?

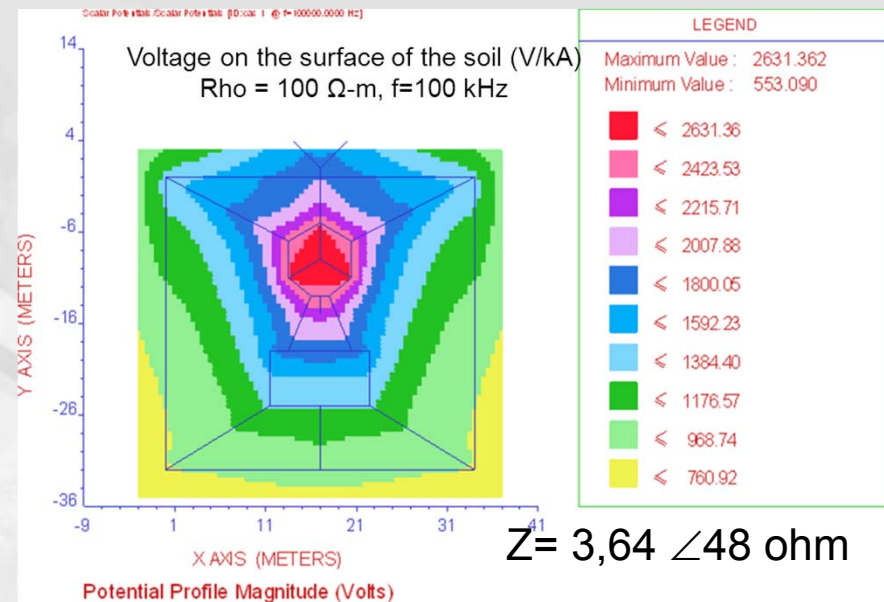
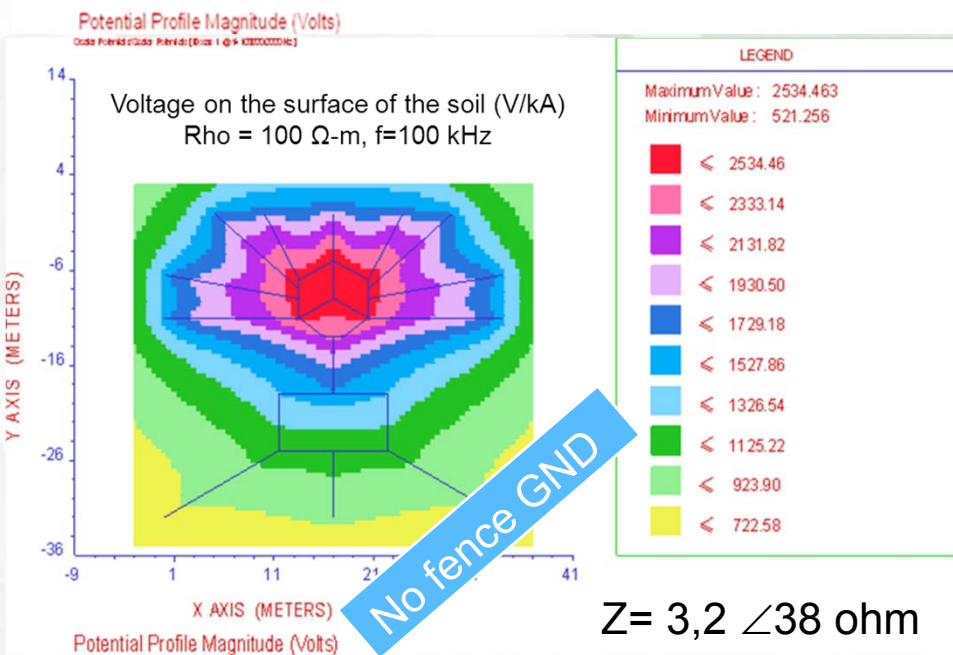
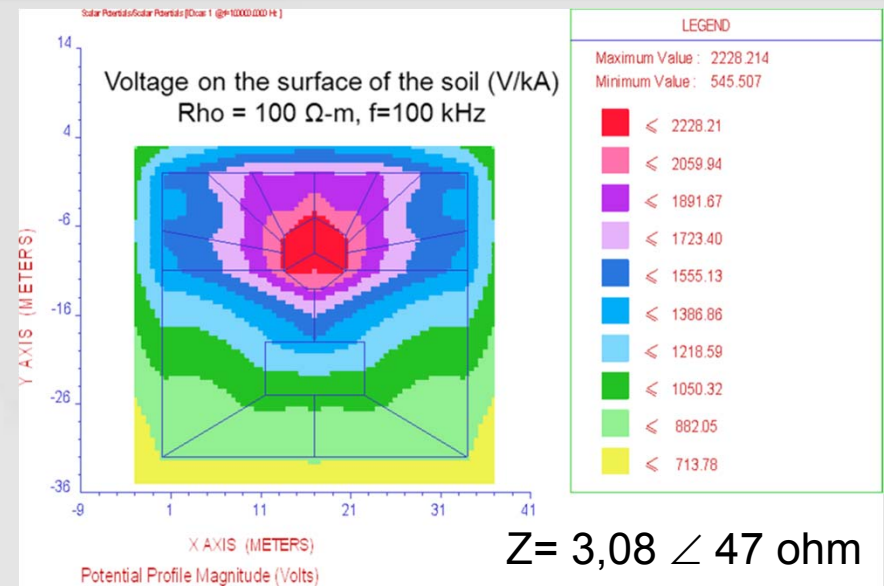
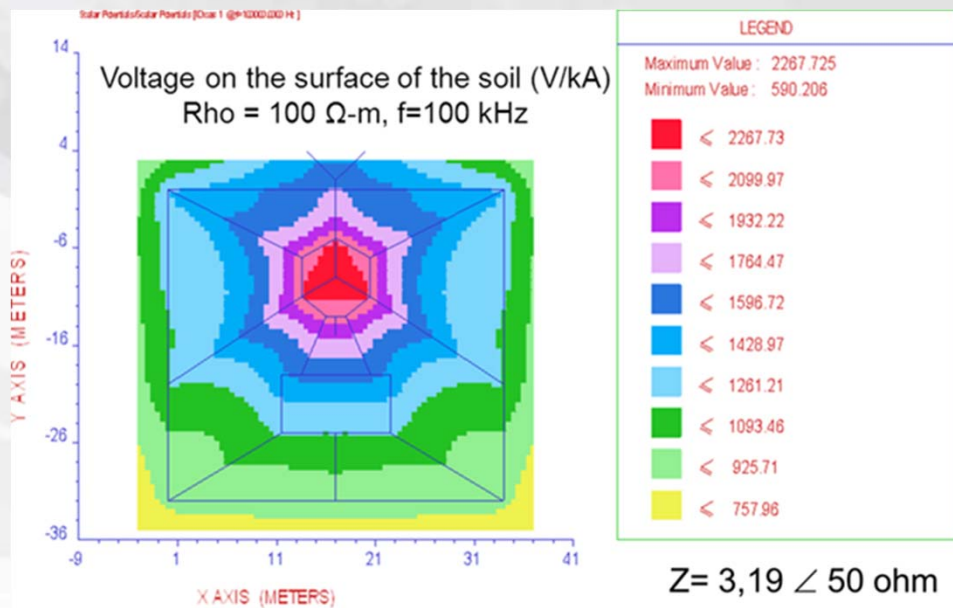
Rho = 100 Ω -m & 10,000 Ω -m, f = 100 Hz



At low frequencies, overall impedance is directly proportional to soil resistivity

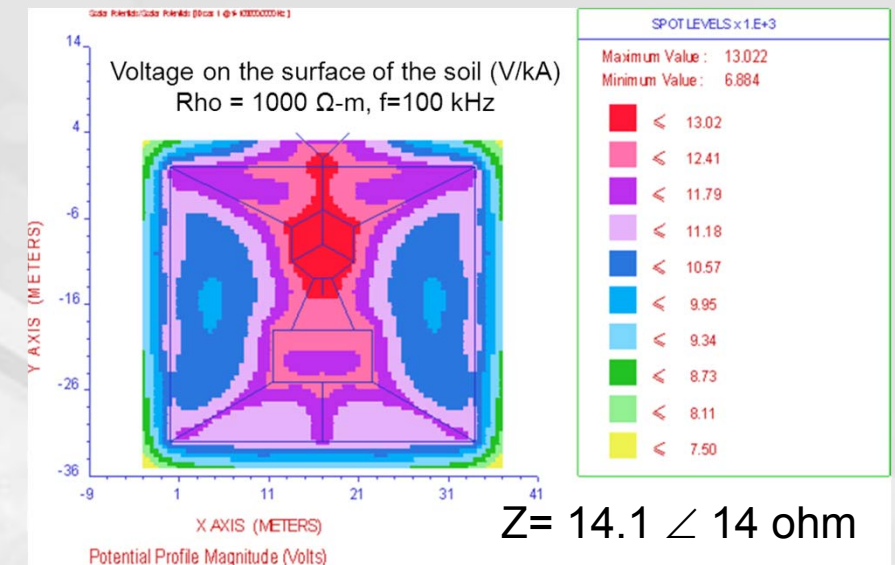
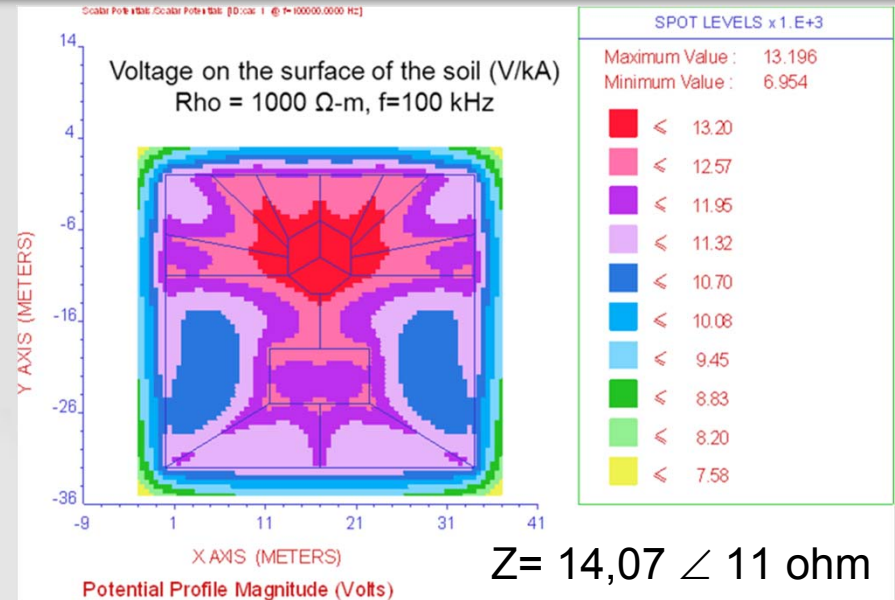
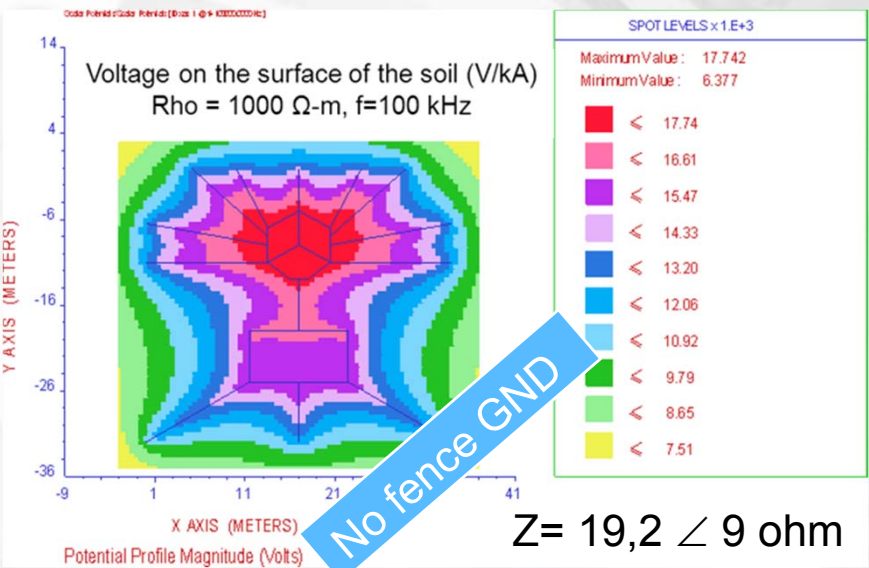
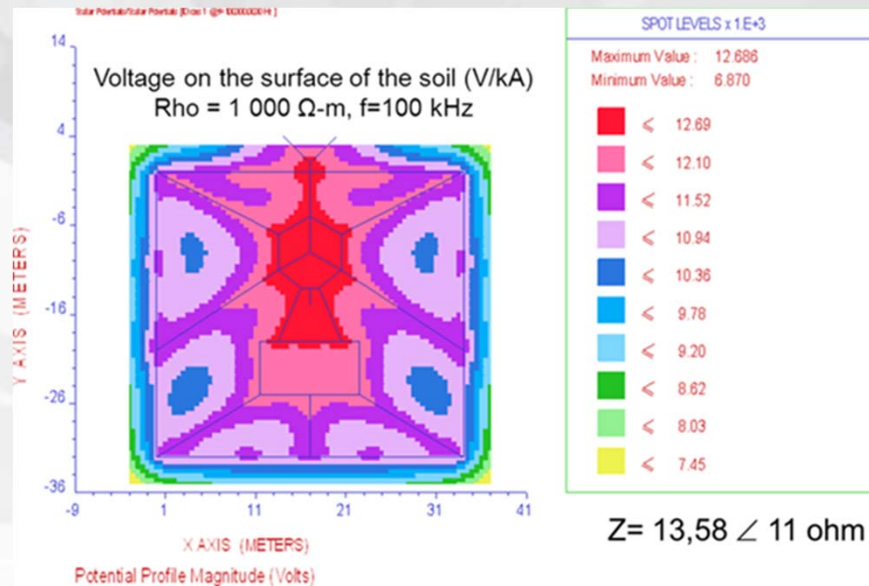
How do grounding models compare?

$\rho = 100 \Omega\text{-m}$, $f = 100 \text{ kHz}$



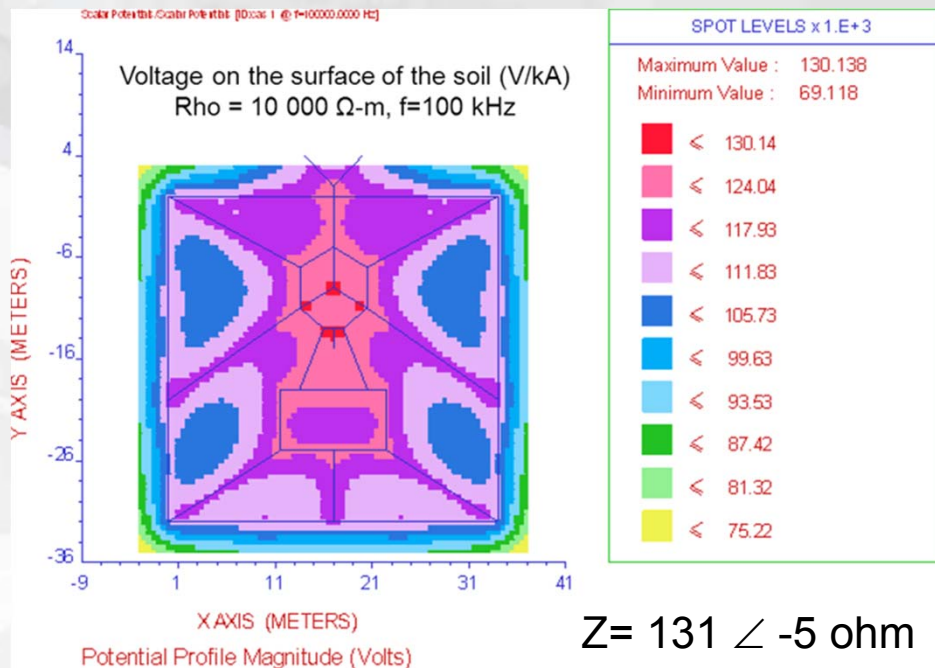
How do grounding models compare?

$\rho = 1,000 \Omega\text{-m}$, $f = 100 \text{ kHz}$

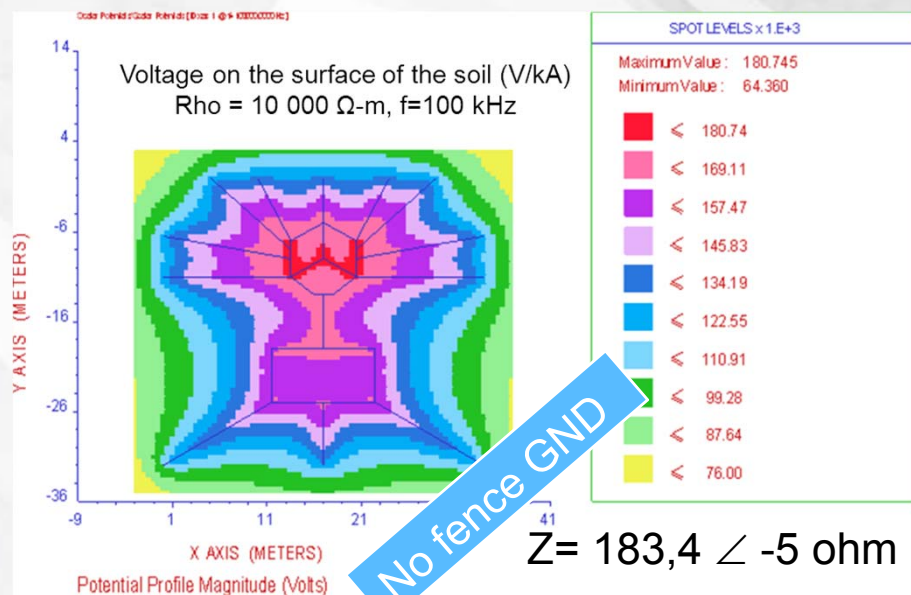


How do grounding models compare?

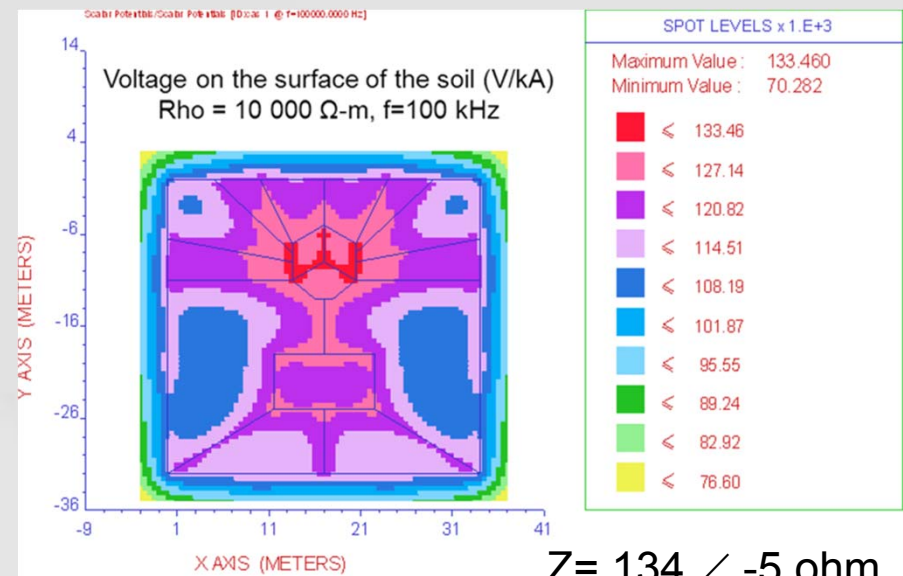
$\rho = 10,000 \Omega\text{-m}$, $f = 100 \text{ kHz}$



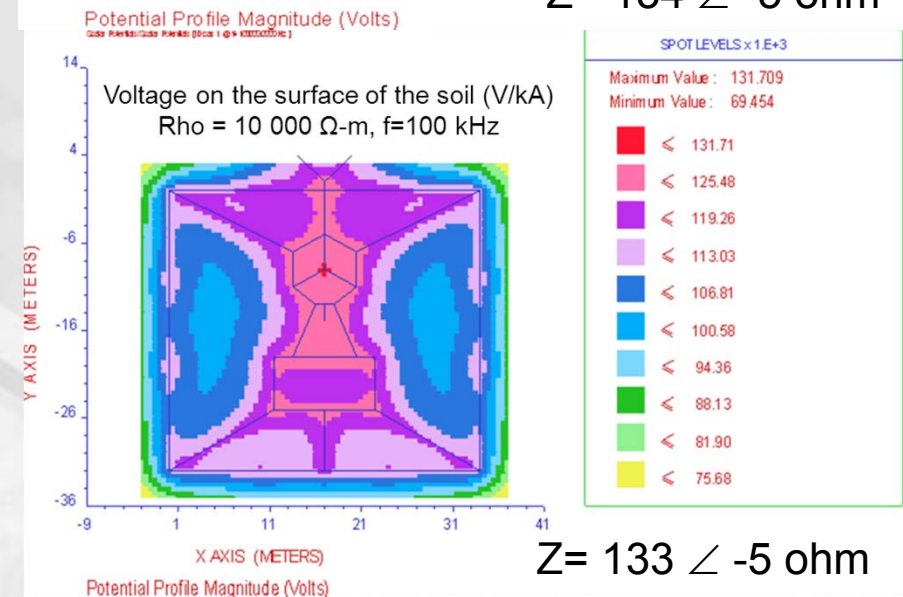
$Z = 131 \angle -5 \text{ ohm}$



$Z = 183,4 \angle -5 \text{ ohm}$



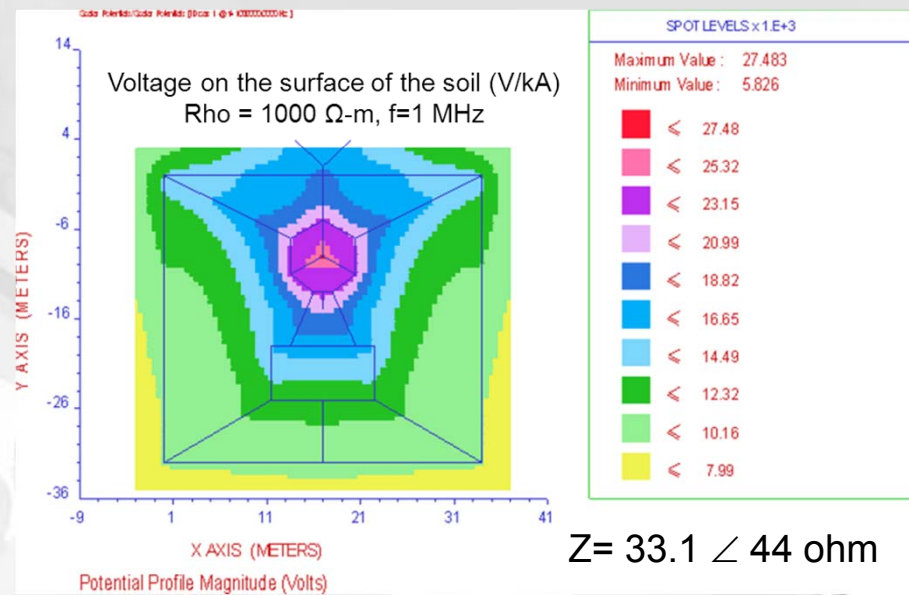
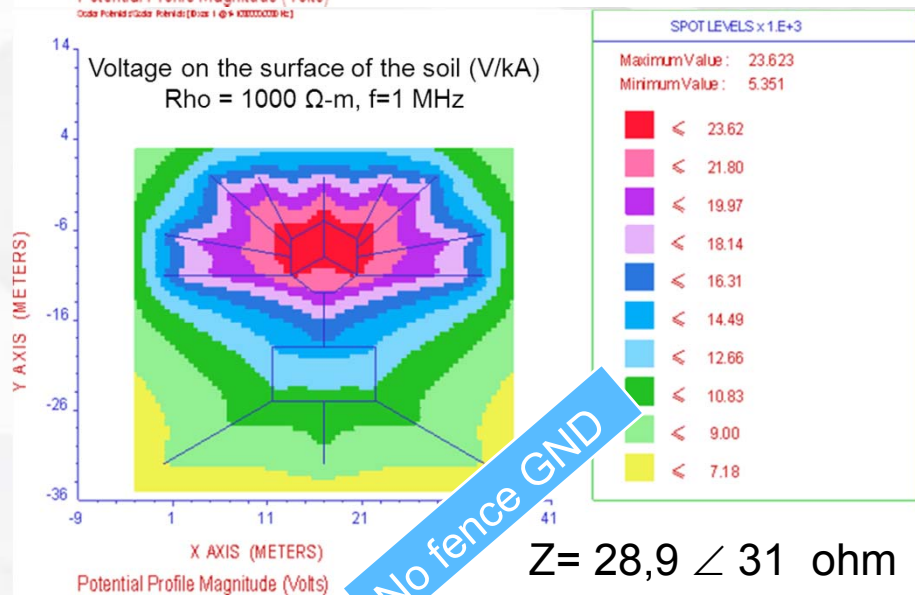
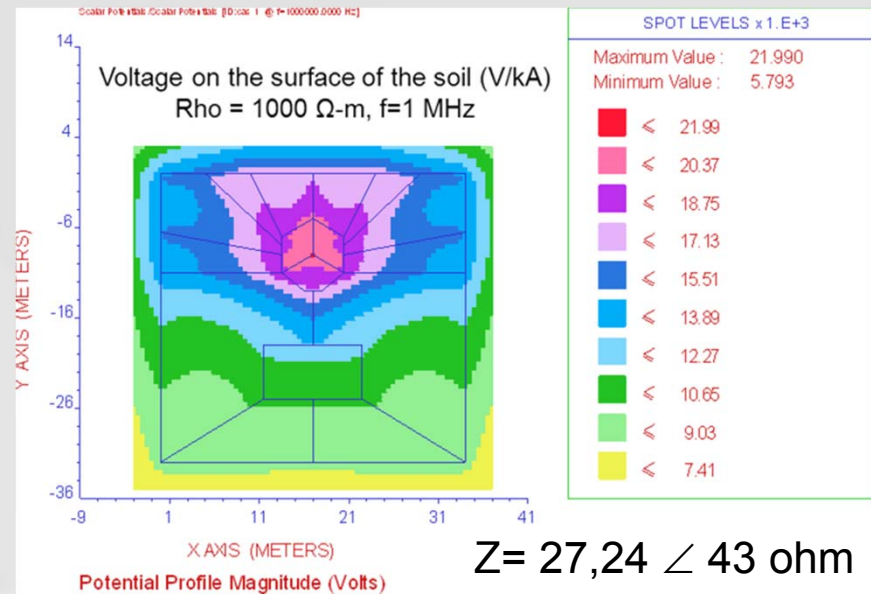
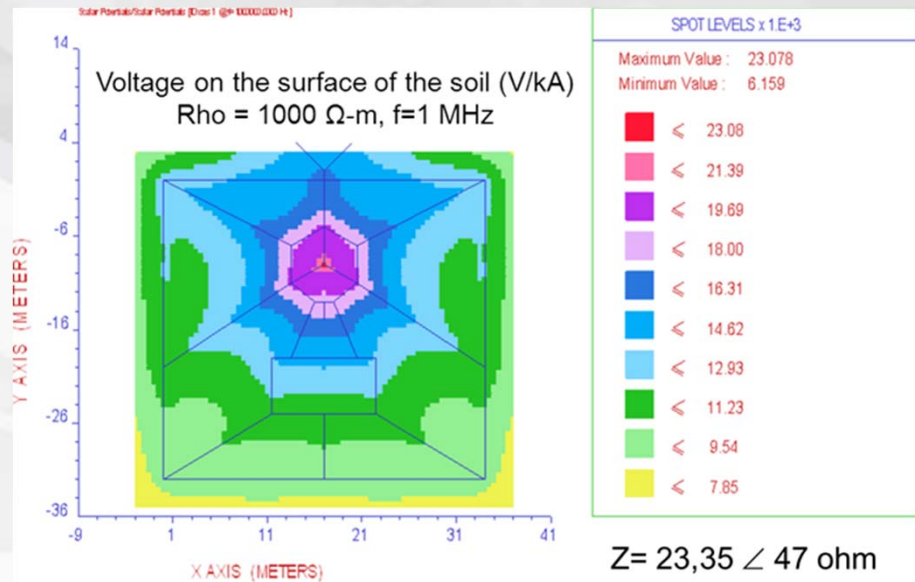
$Z = 134 \angle -5 \text{ ohm}$



$Z = 133 \angle -5 \text{ ohm}$

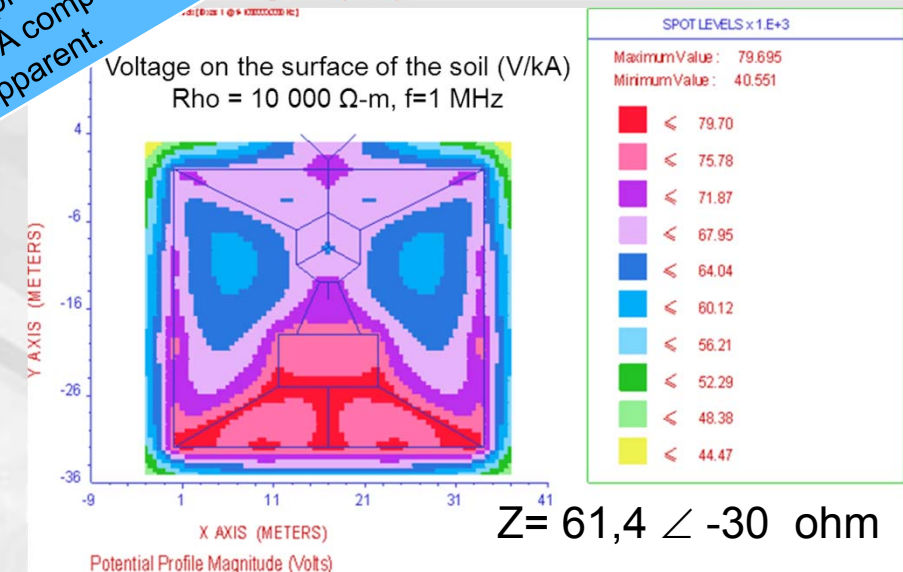
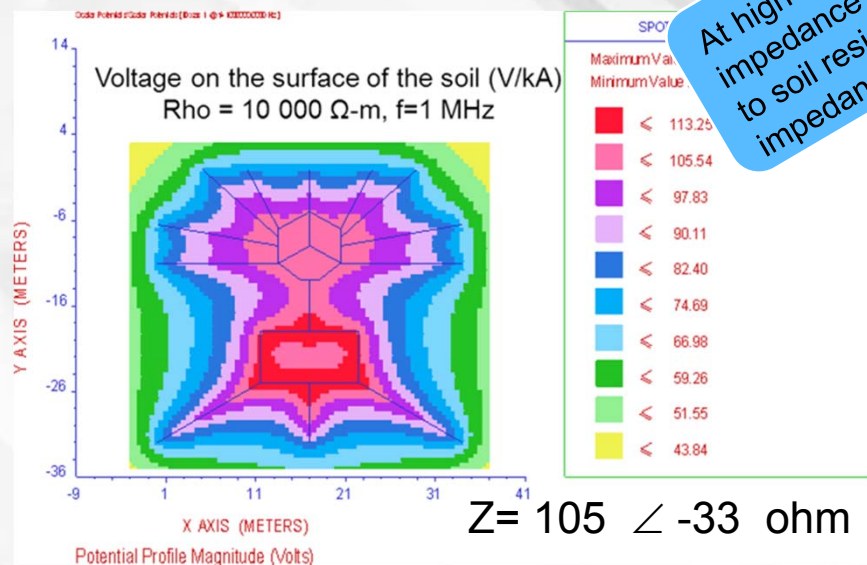
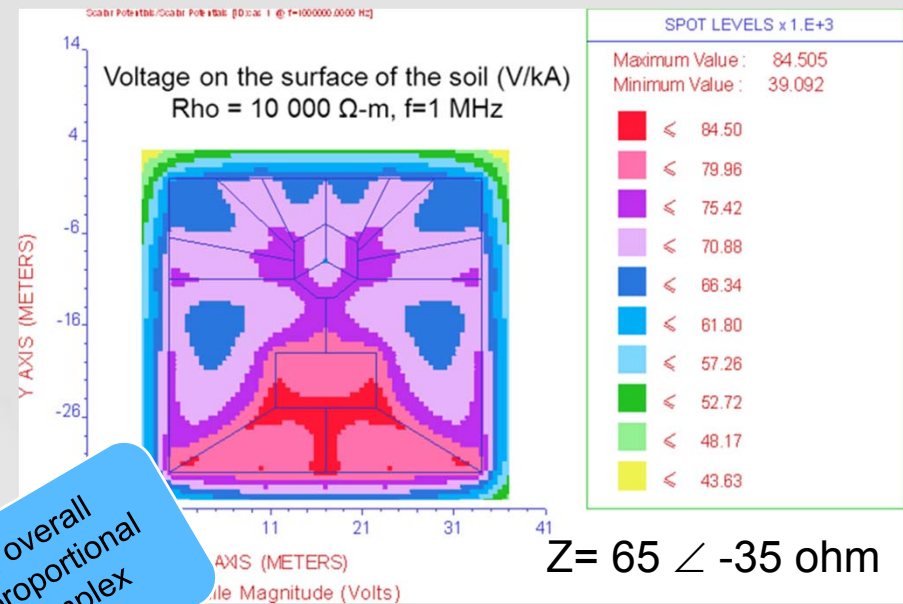
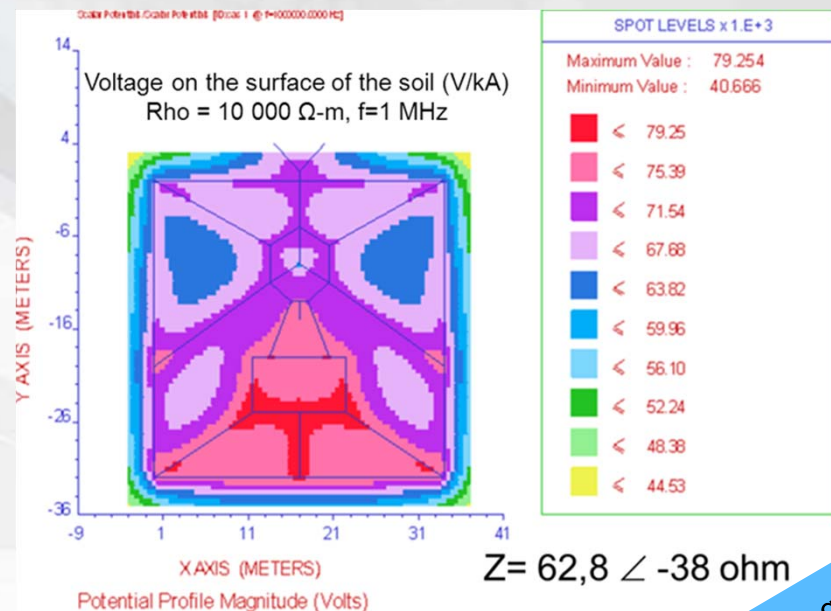
How do grounding models compare?

$\text{Rho} = 1,000 \text{ } \Omega\text{-m}$, $f = 1 \text{ MHz}$



How do grounding models compare?

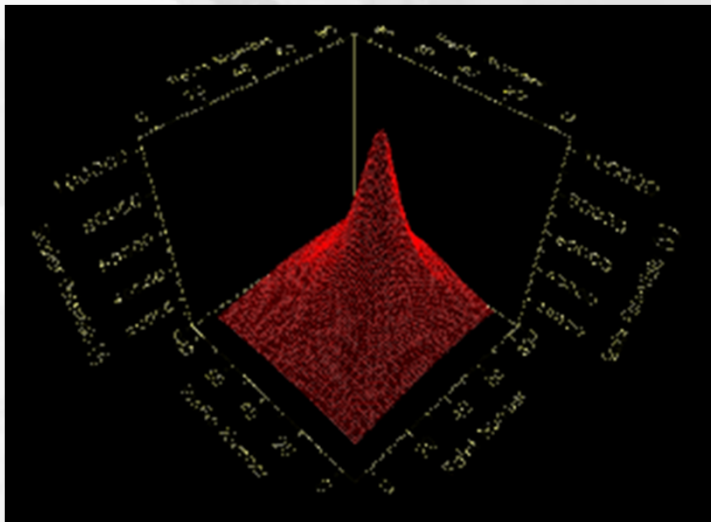
$\text{Rho} = 10,000 \Omega\text{-m}$, $f = 1 \text{ MHz}$



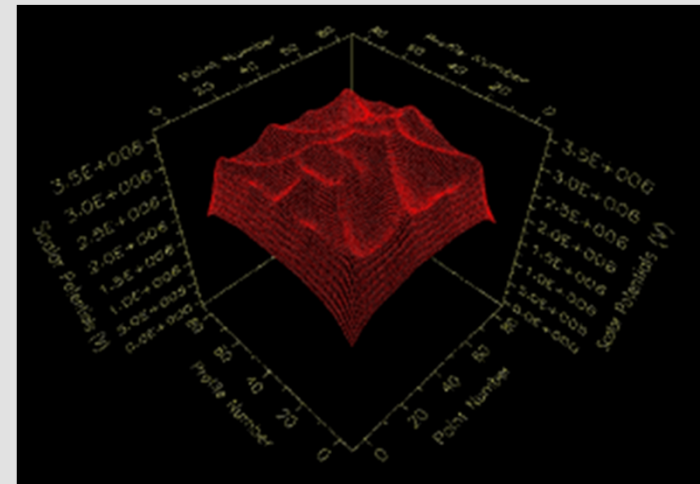
At high frequencies, overall impedance is not proportional to soil resistivity. A complex impedance is apparent.

How do grounding models compare?

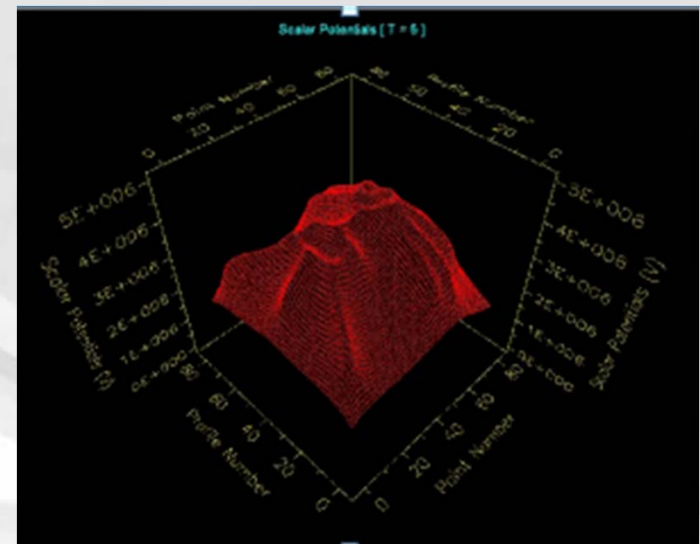
3D models



5 radials, 100Ω-m, 100kHz
With a fence



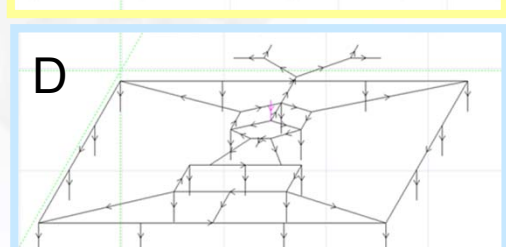
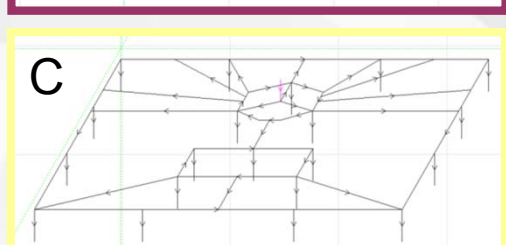
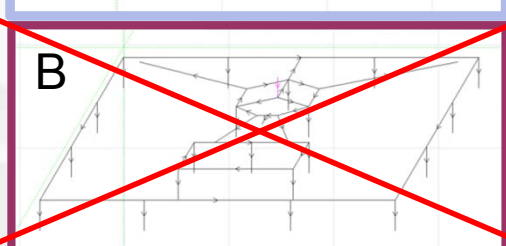
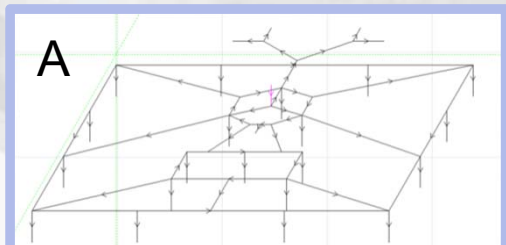
5 radials, 10 000Ω-m, 100kHz
With a fence



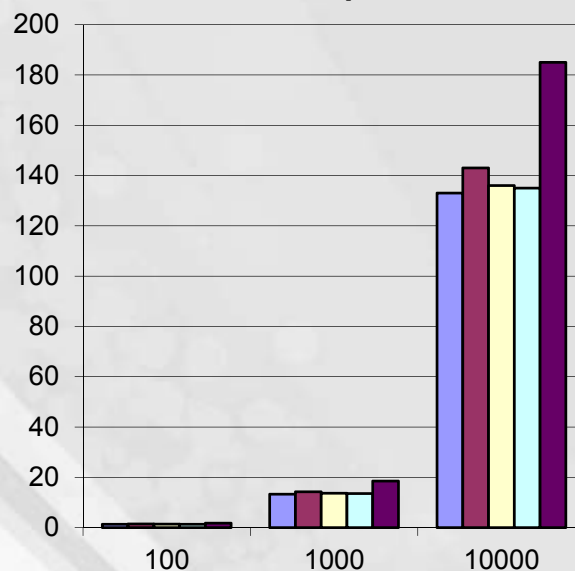
5 radials, 10 000Ω-m, 100kHz
Without a fence

How do grounding models compare?

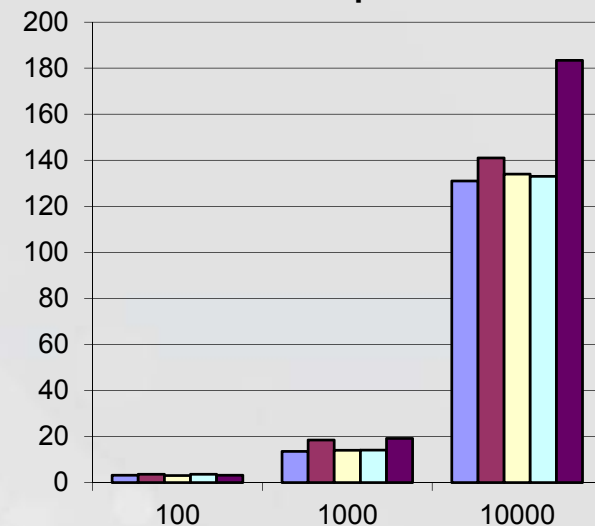
Few or many radials – For what soil type?



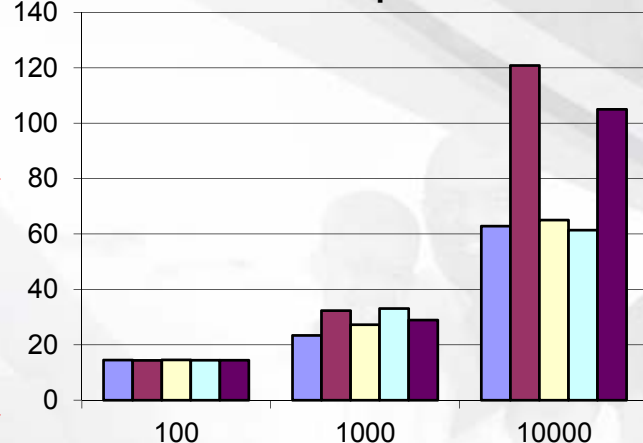
Impedance at 100 Hz



Impedance at 100 kHz



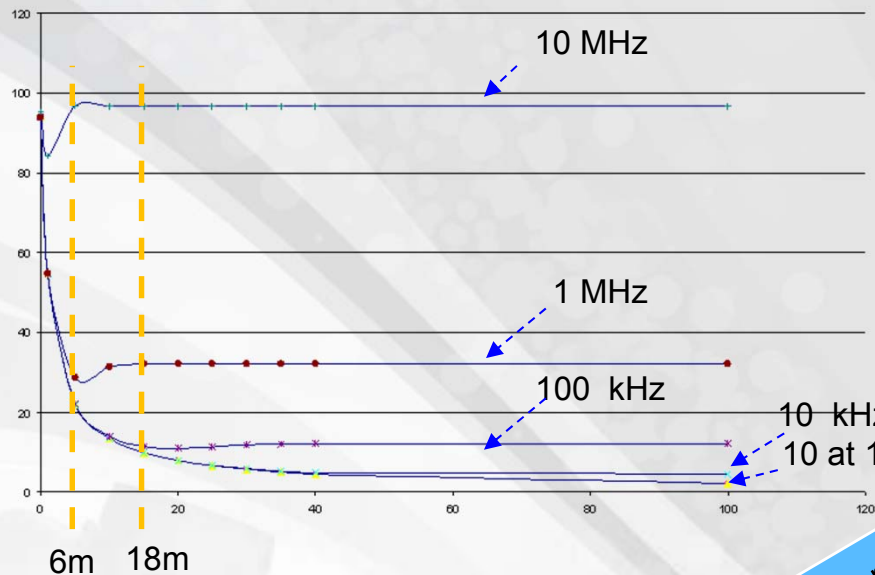
Impedance at 1 MHz



How do grounding models compare?

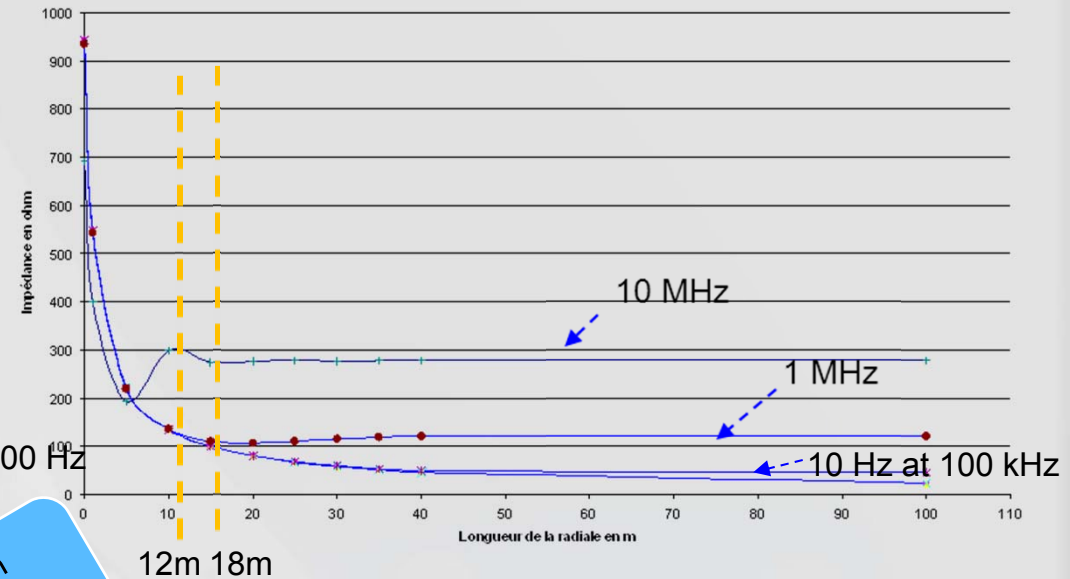
Conductor length – How long is enough?

Effective length as a function of the frequency
Rho 100 Ω -m



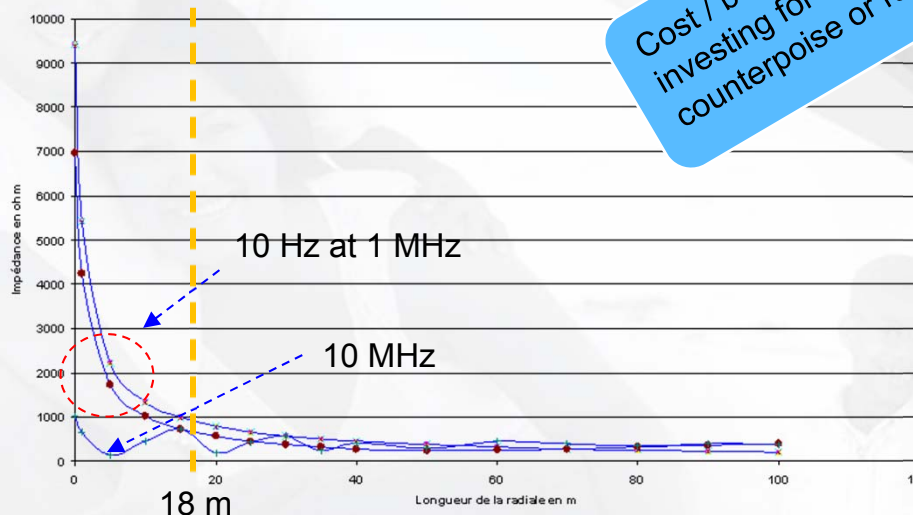
Effective length as a function of the frequency
Rho 1,000 Ω -m

Impédance en fonction de la longueur de la radiale



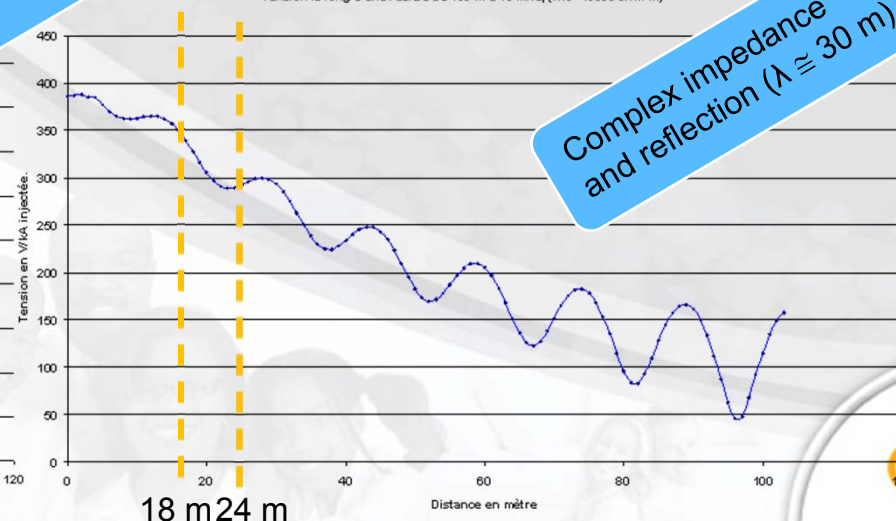
Effective length as a function of the frequency
Rho 10 000 Ω -m

Impédance en fonction de la longueur de la radiale



Voltage along a radial of 100 m
f=10 MHz, Rho 10 000 Ω -m

Tension le long d'une radiale de 100 m à 10 MHz, (rho=10000 oh m-m)



Cost / benefit: Not worth investing for longer counterpoise or radial

Complex impedance and reflection ($\lambda \approx 30$ m)

How do grounding models compare?

Cost effectiveness!

- Equipotentiality is not observed above 100 kHz
- 5 radials are better than 3
 - especially above 100 kHz
 - offers backup in case of conductor theft
 - less expensive than 10
- Connecting the radials to the grounding conductor around the fence improves overall performance when fence is within 18–24 m
- Ground resistivity affects the length of the buried conductor
 - 6 m (min.), in 6 m increments, maximum of 18 m.
- Complex impedance observed at higher frequencies (ex: $61.4 \angle -30^\circ \Omega$)

How do grounding models compare?

Other views! (As presented by Al Martin, ATIS-PEG-2013)



- IEC 61312-1 (Protection against lightning electromagnetic impulse – Part 1, General principles)
 - Generally ground rods are expected to behave like resistors.
- V. Rakov and M. Uman (ICLRT – Camp Blanding (FL), USA)
 - Concluded that ground rods (systems') also have reactive element that may change the rise time of a surge at high frequencies.
 - Short rods ($\leq 3\text{m}$) resemble a parallel RC circuit (lossy capacitors) influenced by p ;
 - Long rods ($\approx 30\text{m}$) resemble a series RL circuit influenced by p .
 - A long ground rod contributes to decrease the specific energy (I^2t) of a surge by directing the high amplitude low-frequency content to ground.
 - At higher frequencies (fast rising surges), ground rod length can lead to potentially damaging voltage spikes.

How grounding models compare



Environment
Canada

Safety: There is no safe place outdoors during a thunderstorm!

- Do not use the tower structure as a shelter;
- Do not touch or be close to the fence during a storm;
- If caught outside do not stand near tall objects or anything made of metal;
- Avoid using a telephone that is connected to a landline;
- Once in a safe location, remain there for 30 minutes after the last rumble of thunder is heard before resuming your outdoor activities.



Conclusion



- Being aware \approx Better grounding
- Modeling \approx Standards
- Addressing risks \approx Security for all

Questions?

Merci!



Bibliography

- QUÉBEC CONSTRUCTION CODE, Chapter V – Electricity – 2012
- Utilisation du code électrique, Polytechnique – Montréal - 2010
- Hydro-Québec – SN-12.3b (Réalisation et contrôle de la qualité des connexions dans les réseaux de terre)
- Hydro-Québec – SN-T-12.01.01.B (Mise à la terre, Installations de télécommunications)
- Hydro-Québec – GT-T-12.01.03.D (Mise à la terre, Installations de télécommunications)
- Hydro-Québec – La foudre: Sa génération, ses effets et notre protection, Eugène Lambert, Eng. – 2006
- T1-313-2003 (Electrical Protection for Telecommunications COs and Similar Facilities)
- EDSPIC:340 (Étude des risques de défaillance d'un réseau de télécommunications soumis aux effets directs ou indirects de la foudre, José Ribeiro)
- Wikipedia – Lightning
- Thor vs. la Masse, VA2J0T-2008
- Lightning & Transients, R. Briët, Ph.D. – ITEM, 2000
- Électrotechnique – Mesures 735, 2001
- Foudre et tension de pas, Frédéric Elie, 2005
- Earthing Fundamentals: Lightning & Surge Technologies
- Transient response of shielded substation hit directly by a lightning strike (Dawalibi, Fortin, Li – SES Tech)
- Motorola R56-2005
- IEC 61312-1 (Protection against lightning electromagnetic impulse – part 1 – general principles)